124

FIELD BOOK

740

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON, O.
PHONE 250-X

TABLE FOR REDUCING PERCHES TO FEET AND INCHES.

PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.
1	16.6 in.	21	3.46 6 in.	41	6.76.6 in.	61	10.06.6 in.	81	13.36.6 in.
2	33.0	22	3 63.0	42	6.93.0	62	10.23.0	82	13.53.0
3	49.6	23	3.79.6	43	7.09.6	63	10.39.6	83	13.69.6
4	66.0	24	3.96.0	44	7.26.0	64	10.56.0	84	13.86.0
5	82.6	25	4 12.6	45	7.42.6	65	10.72.6	85	14.02.6
6	99.0	26	4.29.0	46	7.59.0	66	10.89.0	86	14.19.0
7	1.15.6	27	4.45.6	47	7.75.6	67	11.05.6	87	14.35.6
8	1.32.0	28	4.62.0	48	7.92.0	68	11.22.0	88	14.52.0
9	1.48.6	29	4.78.6	49	8.08.6	69	11.38.6	89	14.68.6
10	1.65.0	30	4.95.0	50	8.25.0	70	11.55.0	90	14.85.0
11	1.81.6	31	5 11.6	51	8.41.6	71	11.71.6	91	15.01.6
12	1.98.0	32	5.28.0	52	8.58.0	72	11.88.0	92	15.18.0
13	2.14.6	33	5.44.6	53	8.74.6	73	12.04.6	93	15.34.6
14	2.31.0	34	5.61.0	54	8.91.0	74	12.21.0	94	15.51.0
15	2.47.6	35	5.77.6	55	9.07.6	75	12.37.6	95	15.67.6
16	2.64.0	36	5.94.0	56	9.24.0	76	12.54.0	96	15.84.0
17	2.80.6	37	6.10.6	57	9.40.6	77	12.70.6	97	16.00.6
18	2.97.0	38	6.27.0	58	9.57.0	78	12.87.0	98	16.17.0
19	3.13.6	39	6.43.6	59	9.73.6	79	13.03.6	99	16.33.6
20	3.30.0	40	6.60.0	60	9.90.0	80	13.20.0	100	16.50.0

B. K. ELLIOTT COMPANY, PITTSBURG, PA.
DRAWING MATERIALS AND SURVEYING INSTRUMENTS

Book 174

Newbury Township

SOULES COR. Rd.

Soules Cor's = ℄ Bell St & Chillicothe Rd.

All stakes set 20' Offset from ℄ to the Left unless otherwise noted.

BELL ST → CH #10 IN NEWBURY Pg 1-23

BELL ST. Sec. D E & F 1950

Pro File PS 24-46

Align. 70-79

BELL ST GRADE STAKES FOR BUTTON DITCH 65

Bench Marks — Pg. 24

Coates Well (N. side Bell St) Pg 68

George Culvert — Pg 64 & 69

LEVELS, BUTTON SWAMP CH. #10 1950 Pg 51-53

BASE TESTS CH. #10 1950 Pg 54

Cross Secs CH #10 Sta 136+0 to 218+0 1950 Pg 55-63

GRADES FOR TILED DITCH CH. #10 W. of BUTTONS 1950 Pg 65

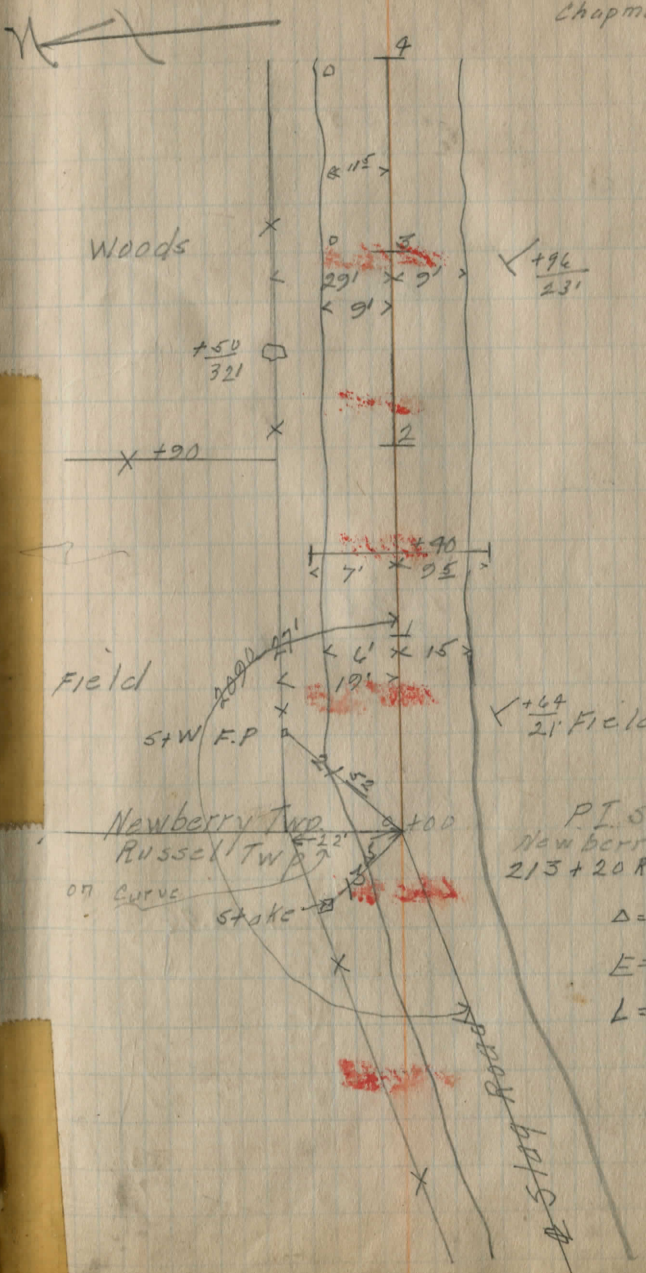
1

1 Nail in East root of 36" Maple
Sta 208 N. Side of Road

Sta	BS	HI	FS	Elev	BM
	4.02	1236.43			1232.41
			12.57	1223.86	
	0.09	1223.95			
		1216.2			
0+00			7.8		
		1214.1			
1+00			2.9		
		1214.1			
1+40 Culv	8 12.6		2.9	10 12.4	
		1213.8			
2+00			10.2		
		1214.0			
3+00			10.0		
		1214.8			
4+00			9.2		
			2.44	1214.43	
	9.39	1223.88			

Dick
Grau
Chapman
7/15/20

1



5+00 1215.5
8.4

6+00 1216.6
7.3

7+00 1217.6
6.3

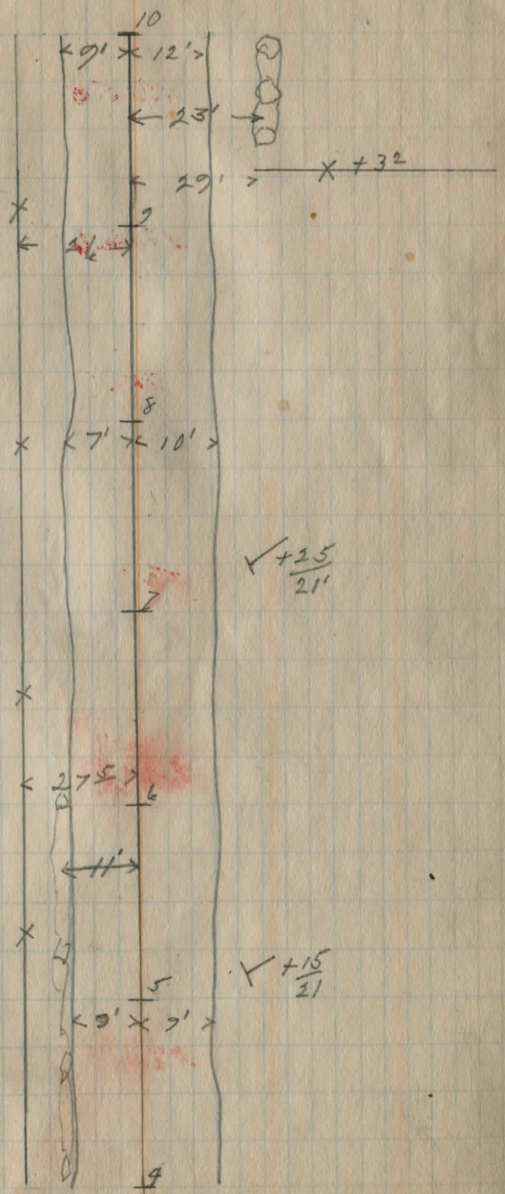
8+00 1219.6
4.3

9+00 1221.6
2.3

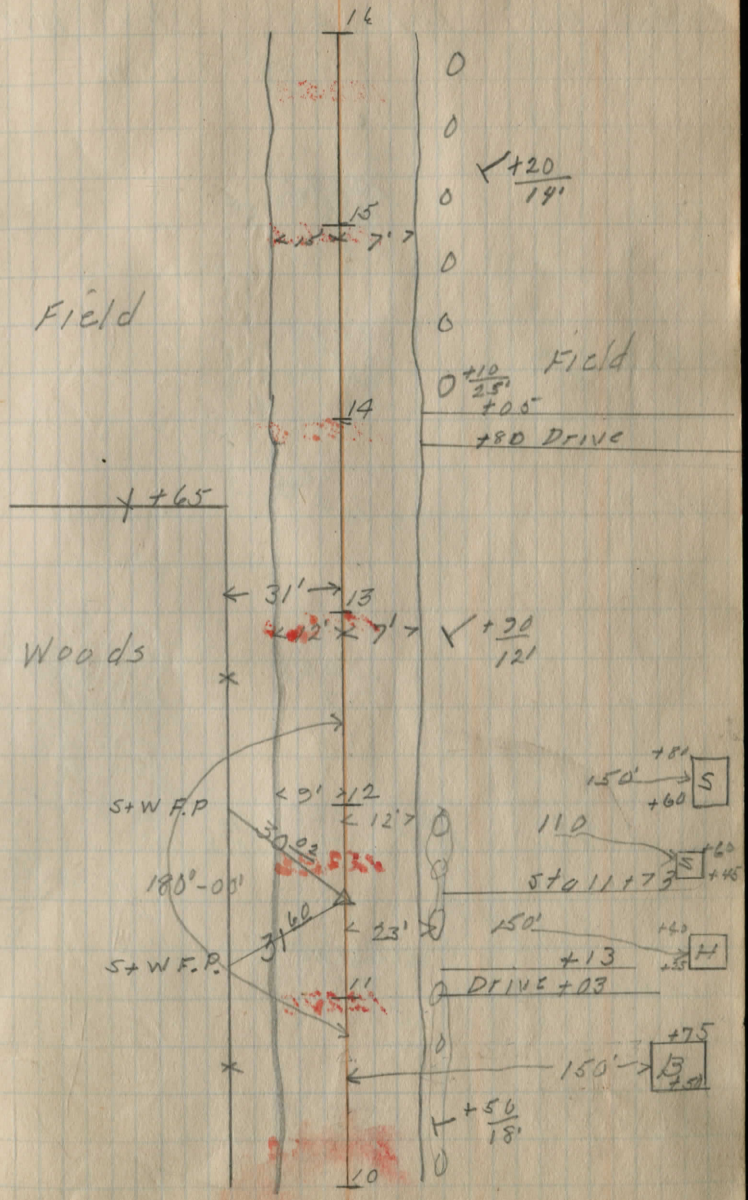
1.44 1222.44

9.68 1232.12

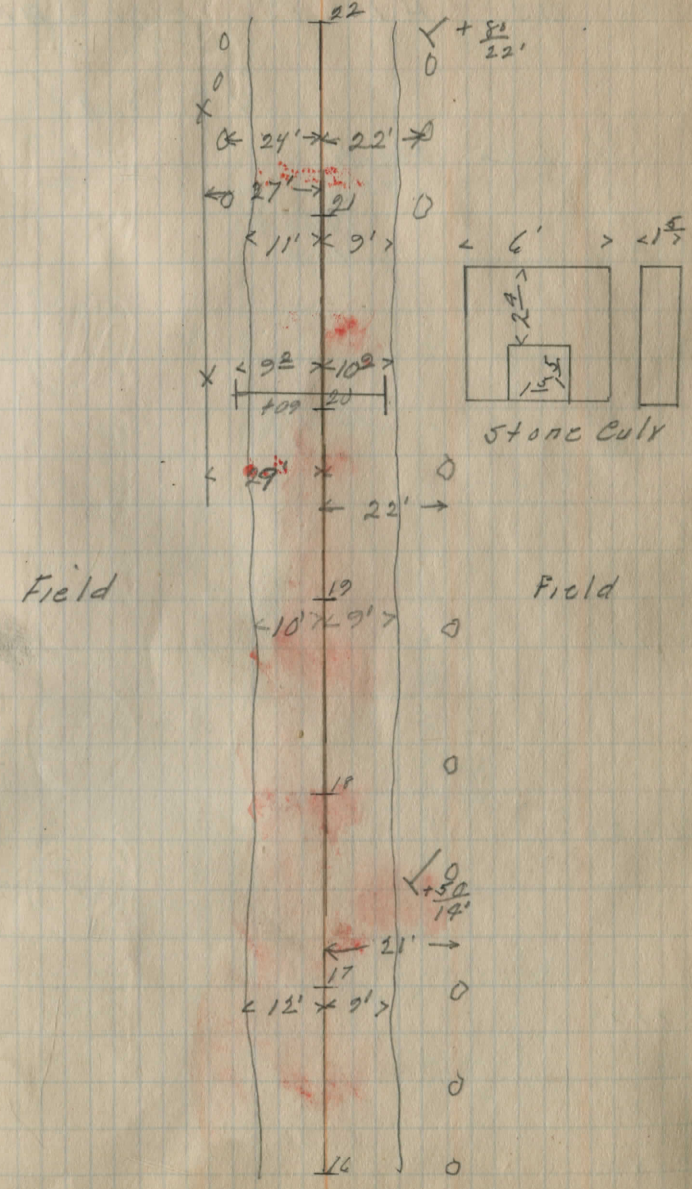
10+05 1223.7
8.4



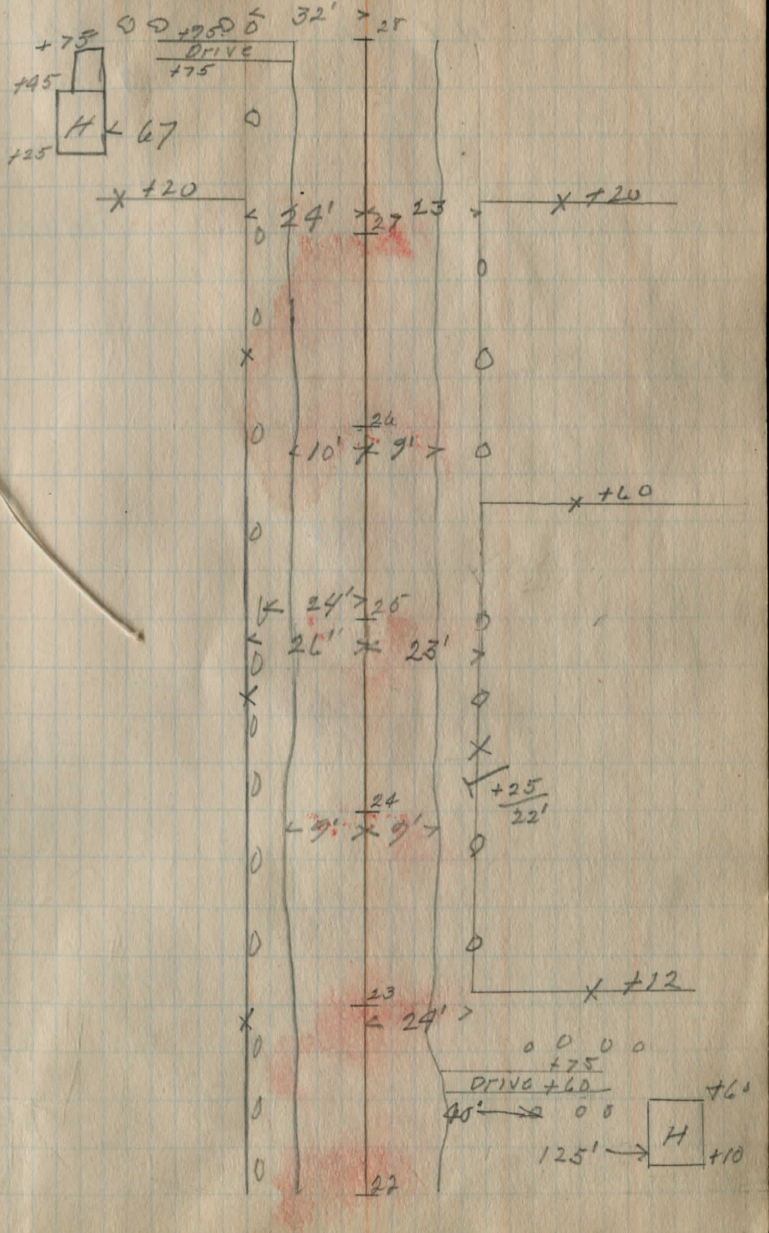
Sta	BS	HI	FS	Elev	BM
11+00			1225.3 6.8		
12+00			1226.6 5.5		
13+00			1227.5 4.6		
14+00			1228.3 3.8		
2 BM Sta 14+02		spike in North Root of Maple 30' Rt. ℄	3.14		1228.98
14+25			1228.6 3.5		
15+00			12270 5.1		
16+06			1225.2 6.9		



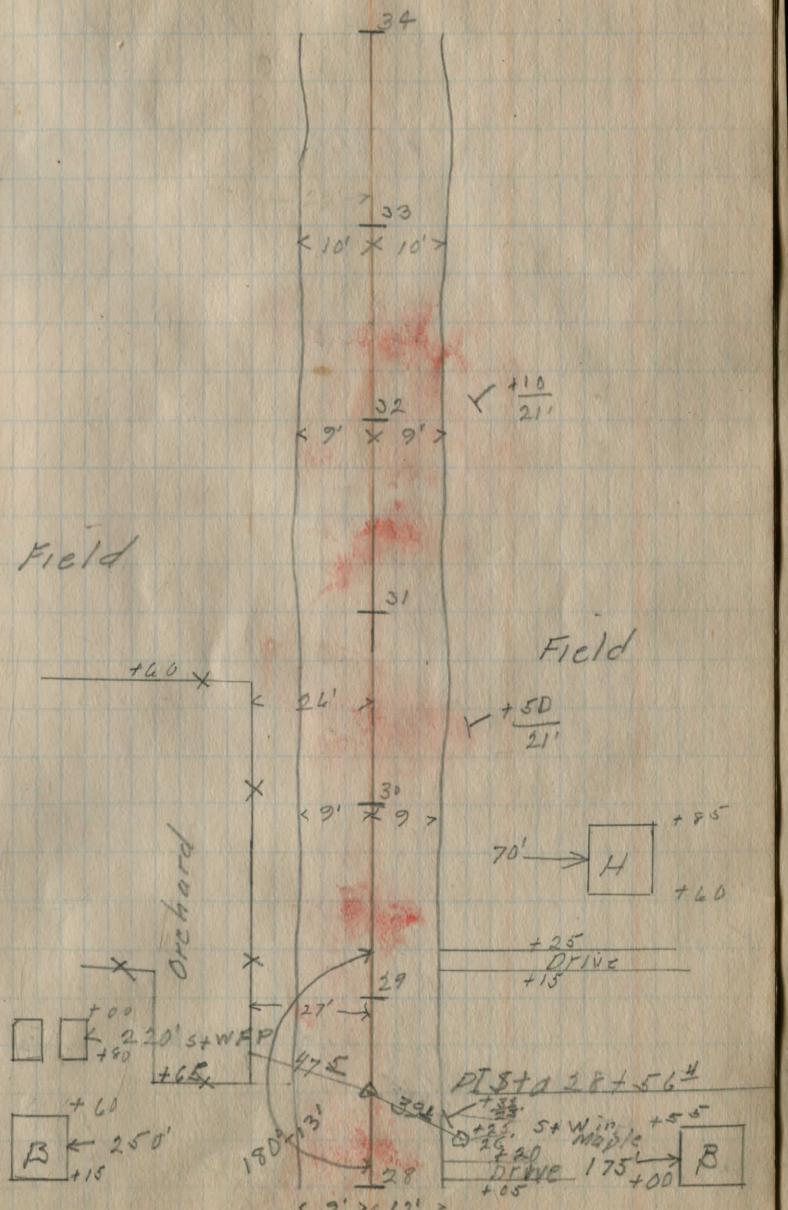
Sta	BS	HI	FS	Elev	BM
			7.00	1225.12	
	2.84	1227.96			
17+00			4.0	1224.0	
18+00			6.5	1221.5	
19+00			7.4	1220.6	
20+00			7.7	1220.1	
20+09 Culv		12 / 10.5	7.9	1220.1	11 / 10.2
21+00			8.2	1219.8	
22+00			8.0	1221.0	



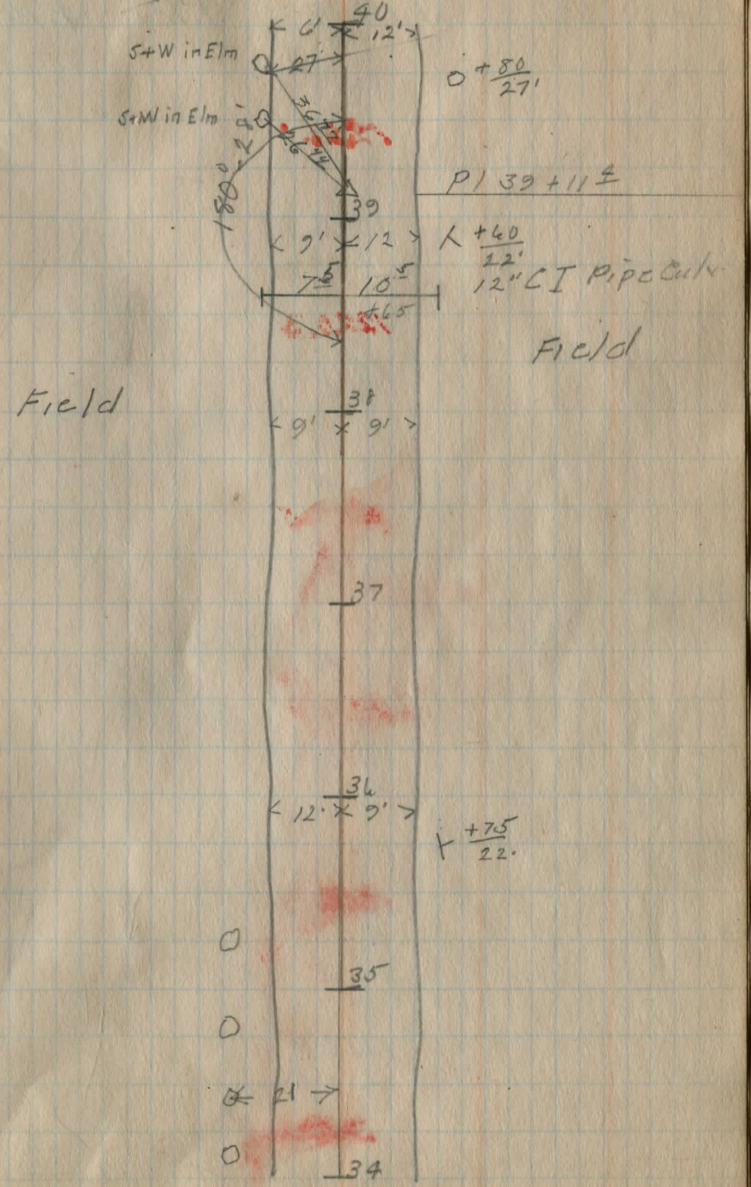
Sta	BS	HI	FS	Elev	BM.
			8.14	1219.52	
	12.22	1232.04			
23+00				1220.5	
			11.5		
24+00				1221.9	
			10.1		
25+00				1222.9	
			9.1		
26+00				1224.5	
			7.5		
27+00				1227.0	
			5.0		
28+06				1230.0	
			2.0		



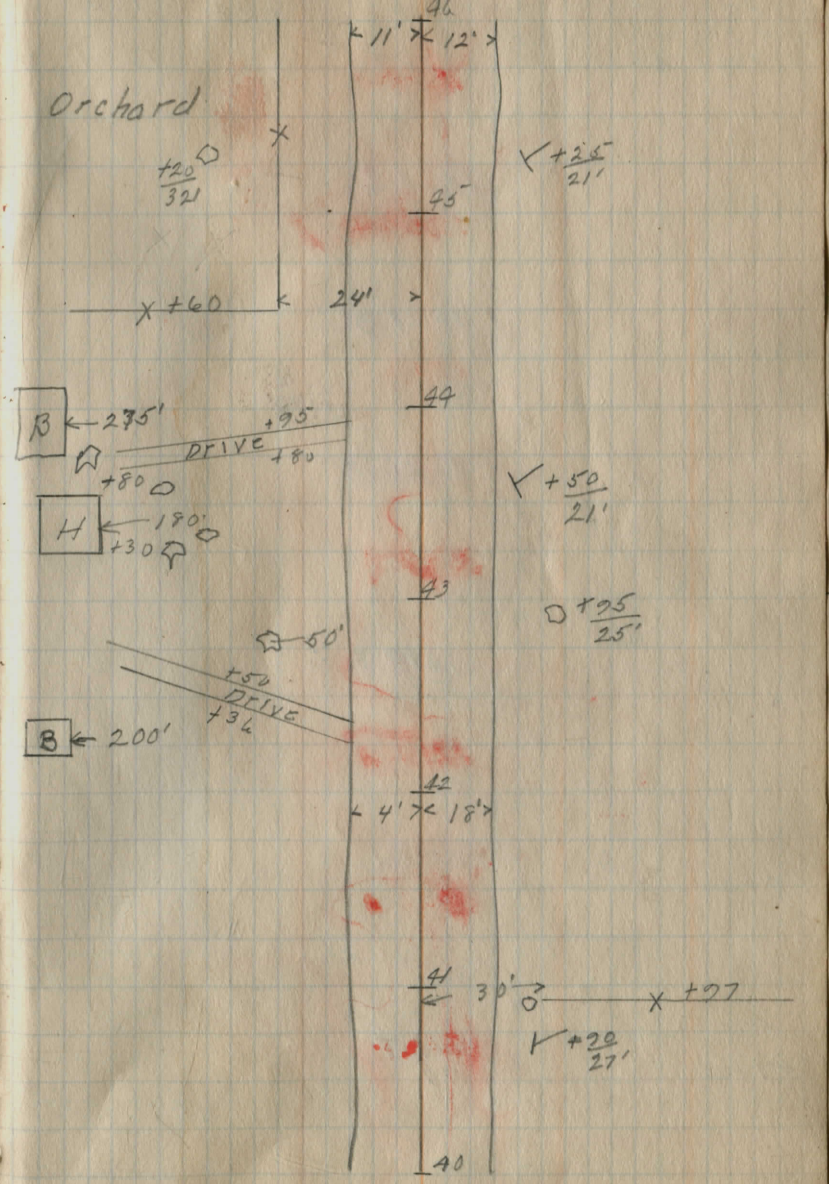
Sta	BS	HI	FS	Elev	BM
			0.92	1231.62	
	3.26	1234.88			
BM sta Spike in Maple 27+90 30' Lt - 2			2.86		1232.02
		1230.9			
29+00			4.0		
		1228.9			
30+00			2.0		
		1225.8			
31+00			9.1		
		1223.5			
32+00			11.4		
			12.06	1222.82	
	2.23	1225.05			
		1222.0			
33+00			3.1		



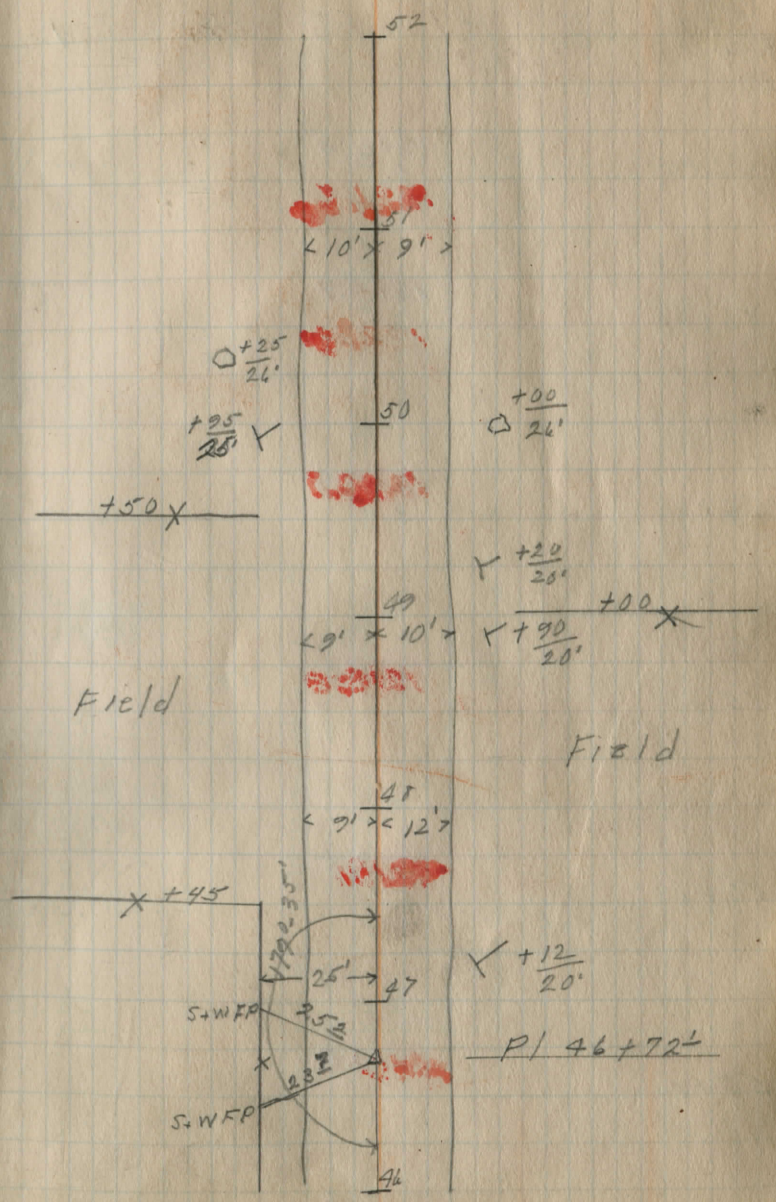
Sta	BS	HI	FS	Elev	BM
34+00		1221.0			
		4.1			
35+00		1220.3			
		4.8			
36+00		1219.5			
		5.6			
37+00		1218.9			
		6.2			
38+00		1218.9			
		6.2			
			6.10	1218.95	
	5.10	1224.05			
38+65 Cul v		1218.8			
		E 6.7	5.3	N 6.3	



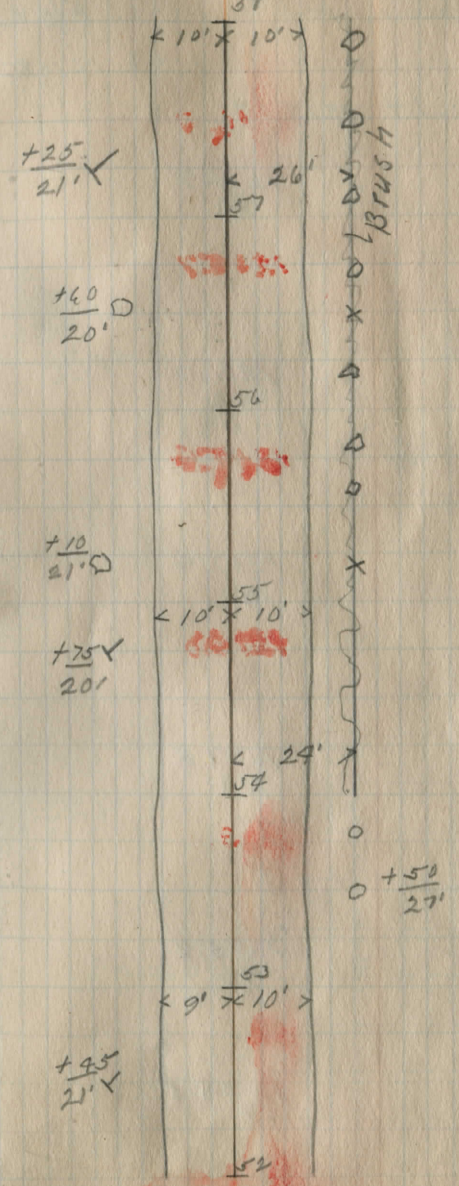
Sta	BS	HI	FS	Elev	BM
39+00		1219.1	5.0		
40+00		1219.0	5.1		
41+00		1219.1	5.0		
42+00		1219.3	4.8		
43+00		1219.8	4.3		
44+00		1220.3	3.8		
45+00		1219.8	3.4		
			2.11	1221.94	
	2.69	1224.63			



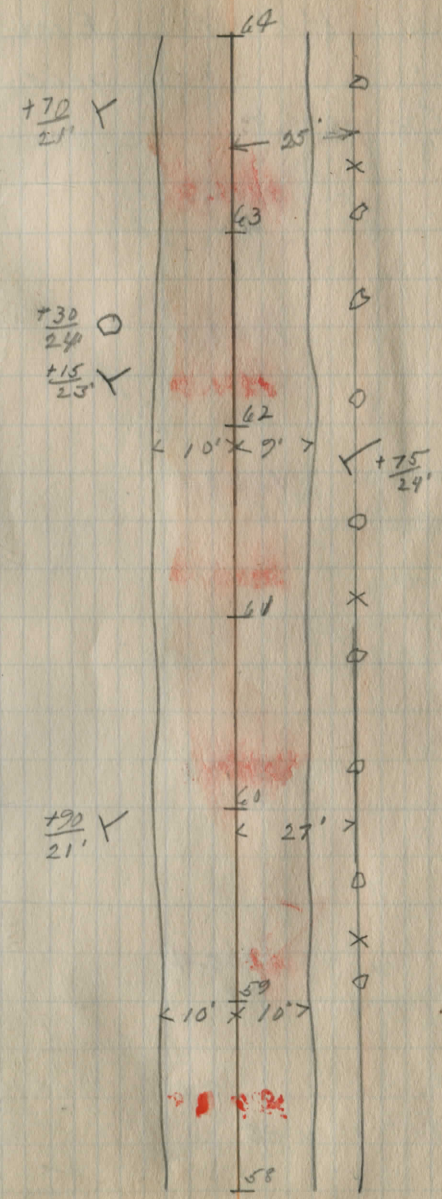
Sta	BS	HI	FS	Elev	BM
BM. Sta 45+20	Nail in Maple 30' Lt. ℄		2.96		1221.67
46+00		1221.7	3.0		
47+00		1221.9	2.7		
48+00		1220.1	4.3		
49+01		1218.8	5.8		
50+00		1218.1	6.5		
51+00		1216.7	7.9		
			8.17	1216.46	
			2.77	1219.23	



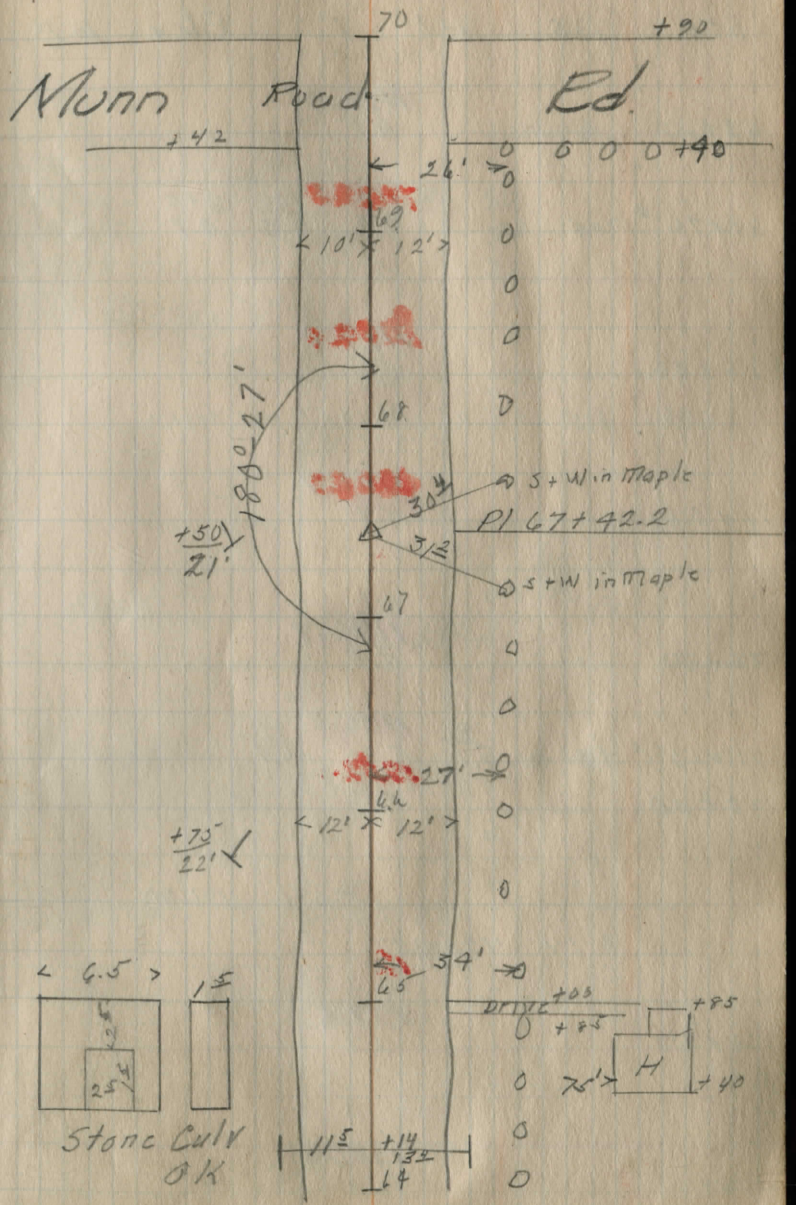
Sta	BS	HI	FS	Elev	BM
BM. 3 45+2					
	52+00	1216.3			
46+		2.7			
	53+00	1215.7			
47+		3.5			
48+	54+00	1215.4			
		3.8			
49+	55+00	1214.0			
		5.2			
50+	56+00	1213.5			
		5.7			
51+	57+00	1213.0			
		6.2			
	58+00	1212.4			
		6.8			



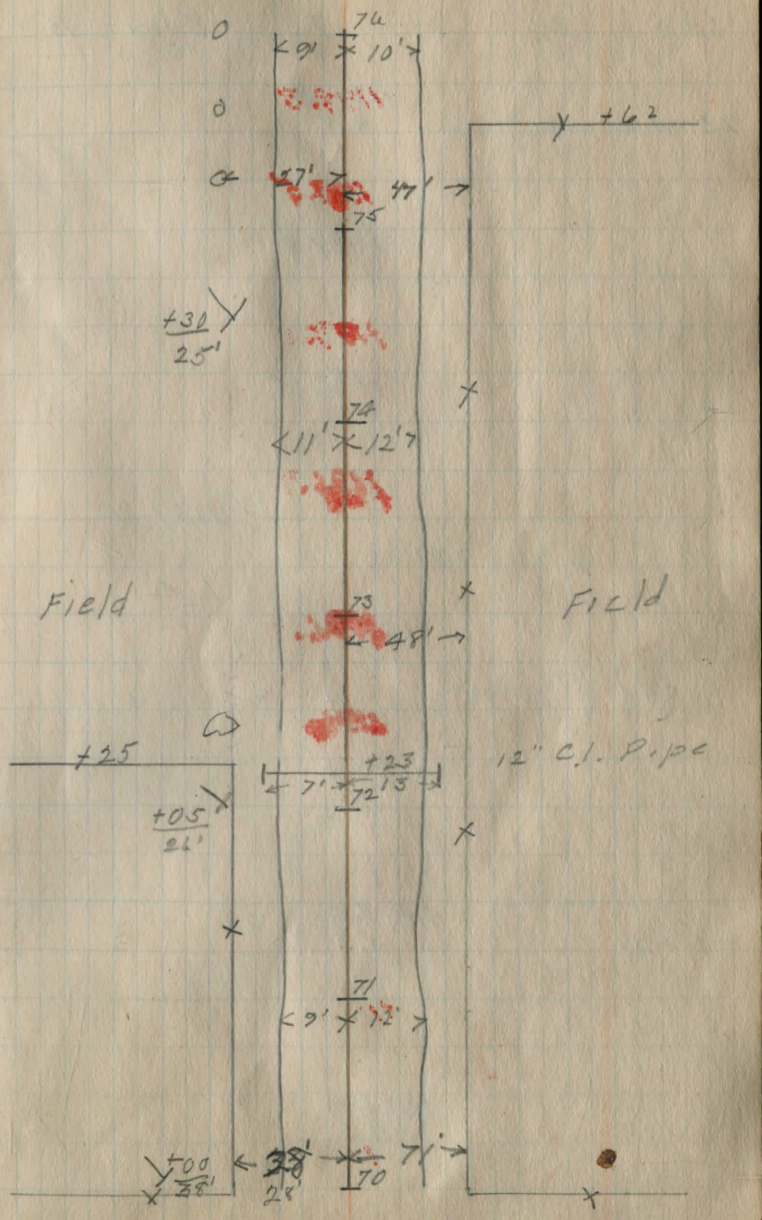
Sta	BS	HI	FS	Elev	BM
			7.34	1211.80	
	3.24	1215.13			
59+00			3.2	1211.9	
60+00			3.4	1211.7	
61+00			4.7	1210.4	
62+00			7.3	1207.8	
63+00			9.9	1205.2	
64+00			10.6	1204.5	



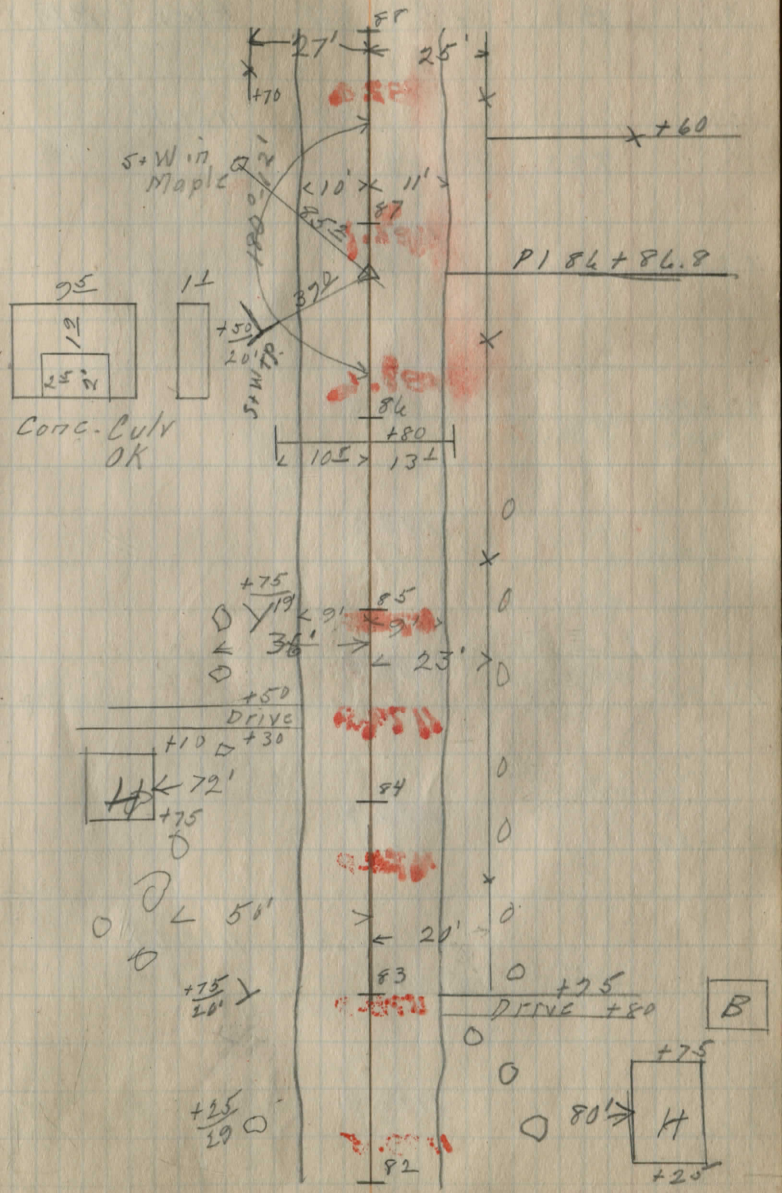
Sta	BS	HI	FS	Elev	BM
			9.56	1205.57	
	3.22	1208.79			
64+15 Culv	12 / 7.2		7204.3 4.5	15 / 7.0	
65+00			1204.0 4.8		
66+00			1204.1 4.7		
BM Sta 566+20	Nail in Maple 27' Rt ℄		2.52	1206.27	
67+00			1202.6 6.2		
68+00			1200.4 8.4		
			8.67	1200.12	
	2.31	1202.43			



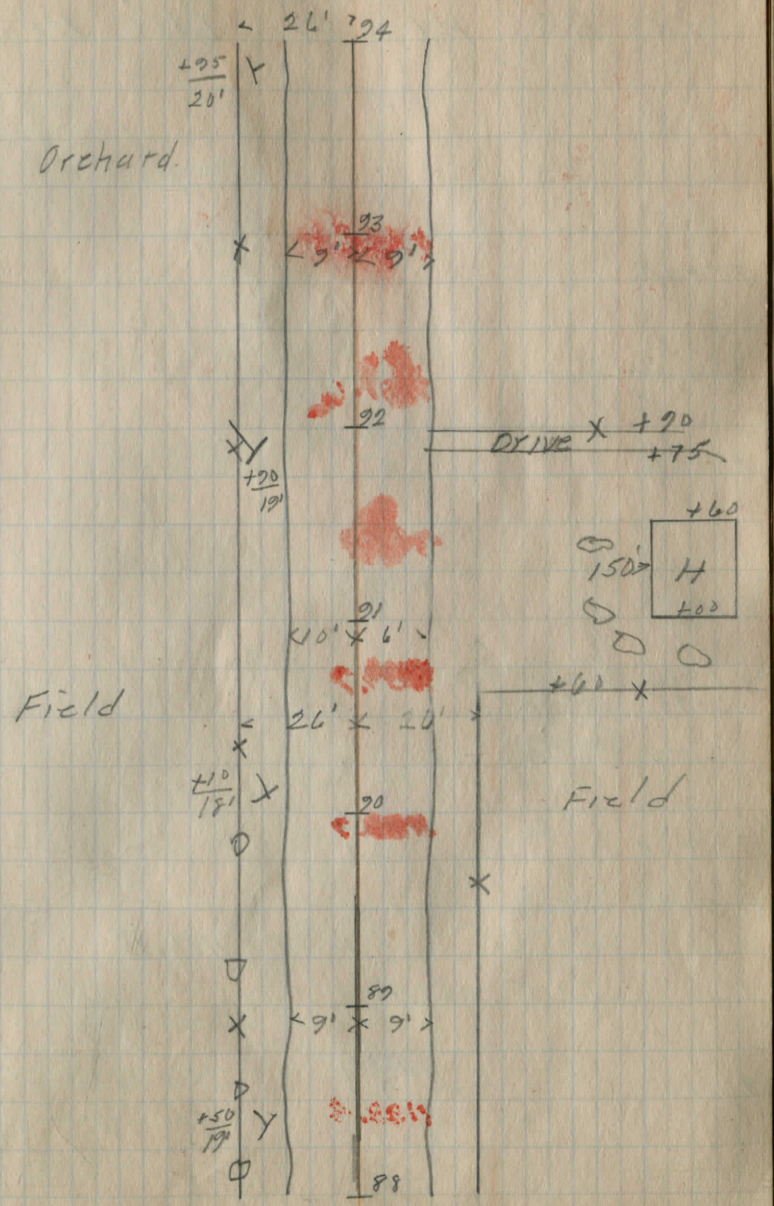
Sta	BS	HI	FS	Elev	BM
69+00				1198.3	
			4.1		
69+70 Road	200 / 4.7	100 / 4.2		1197.5	
			4.9		
			100 / 2.3		
			200 / 0.7		
70+00				1197.0	
			5.4		
±05± SUPPOSED TO BE CULVERT - NOT FOUND					
71+00				1194.7	
			5.7		
72+00				1196.7	
			5.7		
72+13 Cul/V	E / 7.1			1196.8	14 / 4.9
			5.6		
				1196.2	
73+00			5.5		
			5.64	1196.79	
	3.14	1199.93			
73+50				1197.6	
			2.3		
74+00				1196.1	
			3.8		



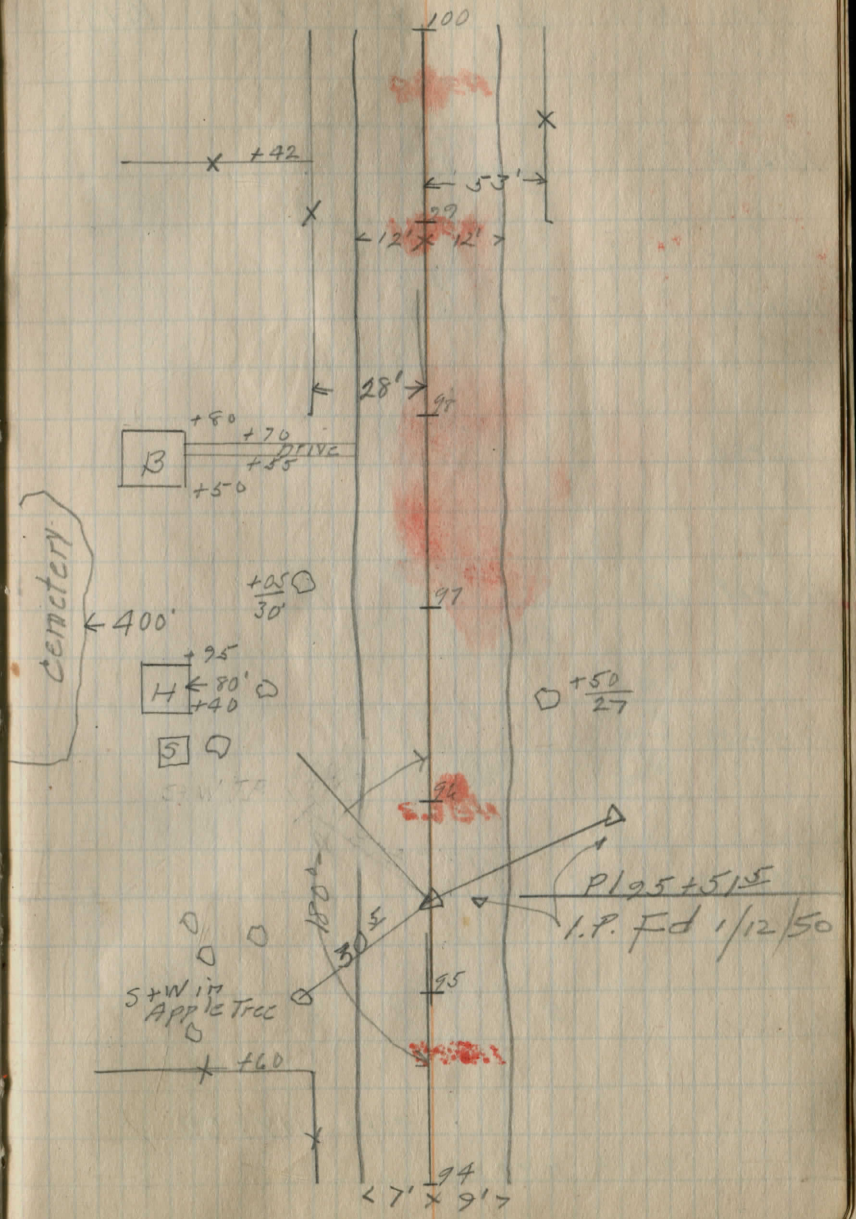
Sta	BS	HI	FS	Elev	131½
82+00		1182.0			
		4.1			
83+00		1186.1			
		5.0			
84+00		1181.6			
		9.5			
			8.98	1182.12	
	2-78	1184.90			
85+00		1179.9			
		5.0			
85+80	11 / 8.0	1179.9	14 / 7.9		
		5.0			
86+00		1178.9			
		6.0			
87+00		1178.9			
		6.0			
88+00		1179.5			
		5.4			



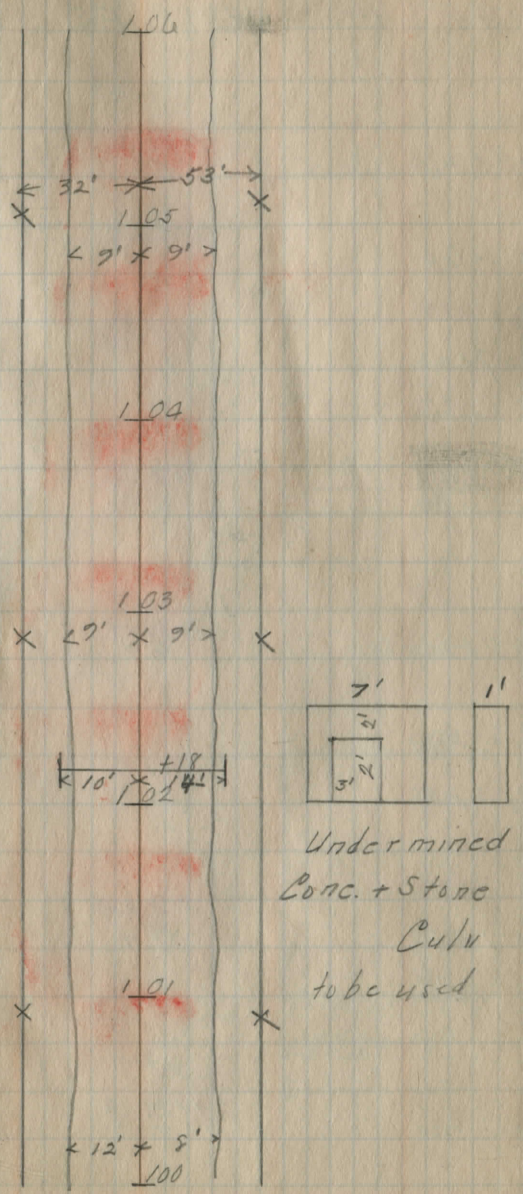
Sta	BS	HI	FS	Elev	BM
			3.76	1181.14	
	7.73	1188.87			
89+00		1181.5	8.4		
90+00		1181.6	7.3		
91+00		1183.0	5.9		
92+00		1184.7	4.2		
93+00		1188.7	0.2		
			0.22	1188.65	
	9.73	1198.38			
94+06		1193.4	5.0		



Sta	BS	HI	FS	Elev	BM
94+75		1195.4			
		3.0			
95+00		1195.1			
		3.3			
96+00		1193.6			
		5.4			
97+00		1190.5			
		7.7			
(e BM sta 94+75	Spike in Maple 30' Rt. ℄ Gone)		5.46		1192.98
98+00		1186.3			
		12.1			
			12.25	1186.13	
	1.65	1187.78			
99+00		1183.3			
		4.5			

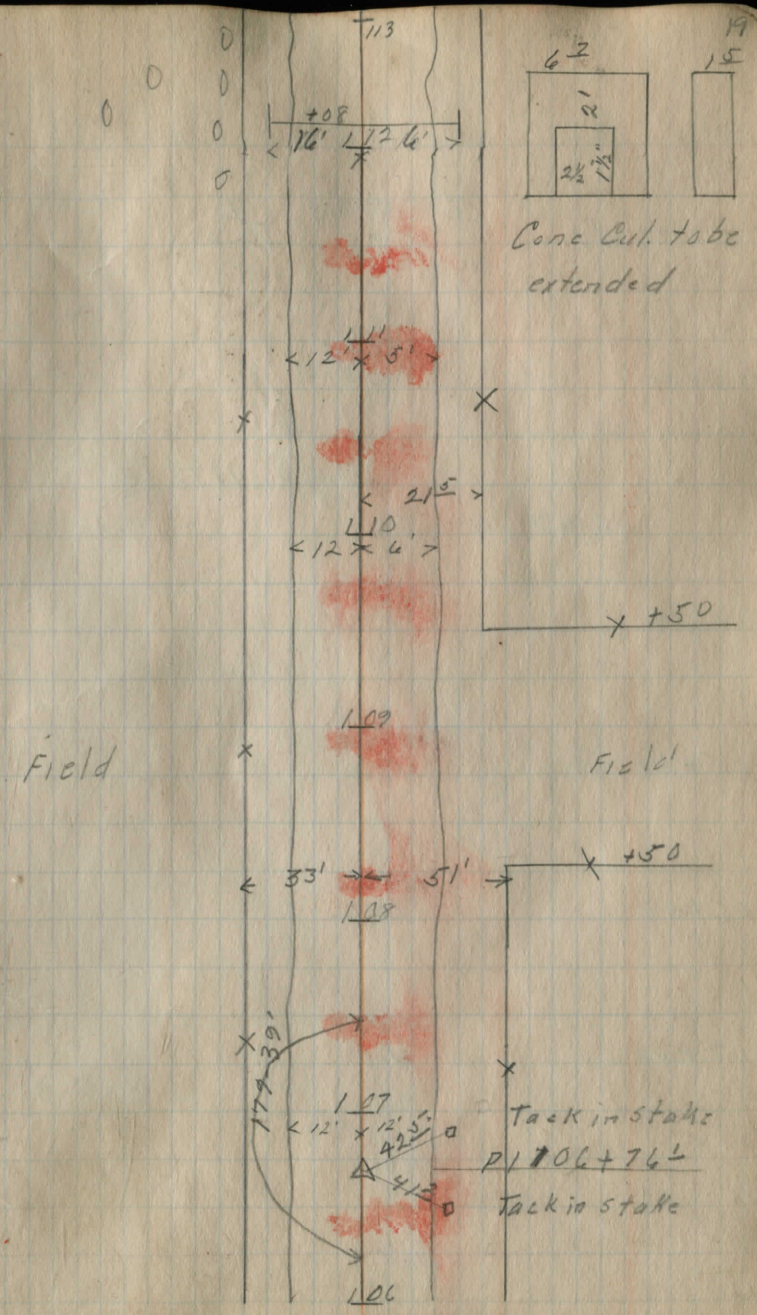


Sta	BS	HI	FS	Elev	BM
100+00		1179.6		8.2	
101+00		1177.4		10.4	
102+00		1176.2		11.6	
102+18 Culv.	11 / 15.0	1175.9	15 / 15.3	11.7	
103+00		1175.3		12.3	
104+00		1175.8		12.0	
105+00		1177.8		10.0	
			8.79	1178.99	
	8.27	1187.26			

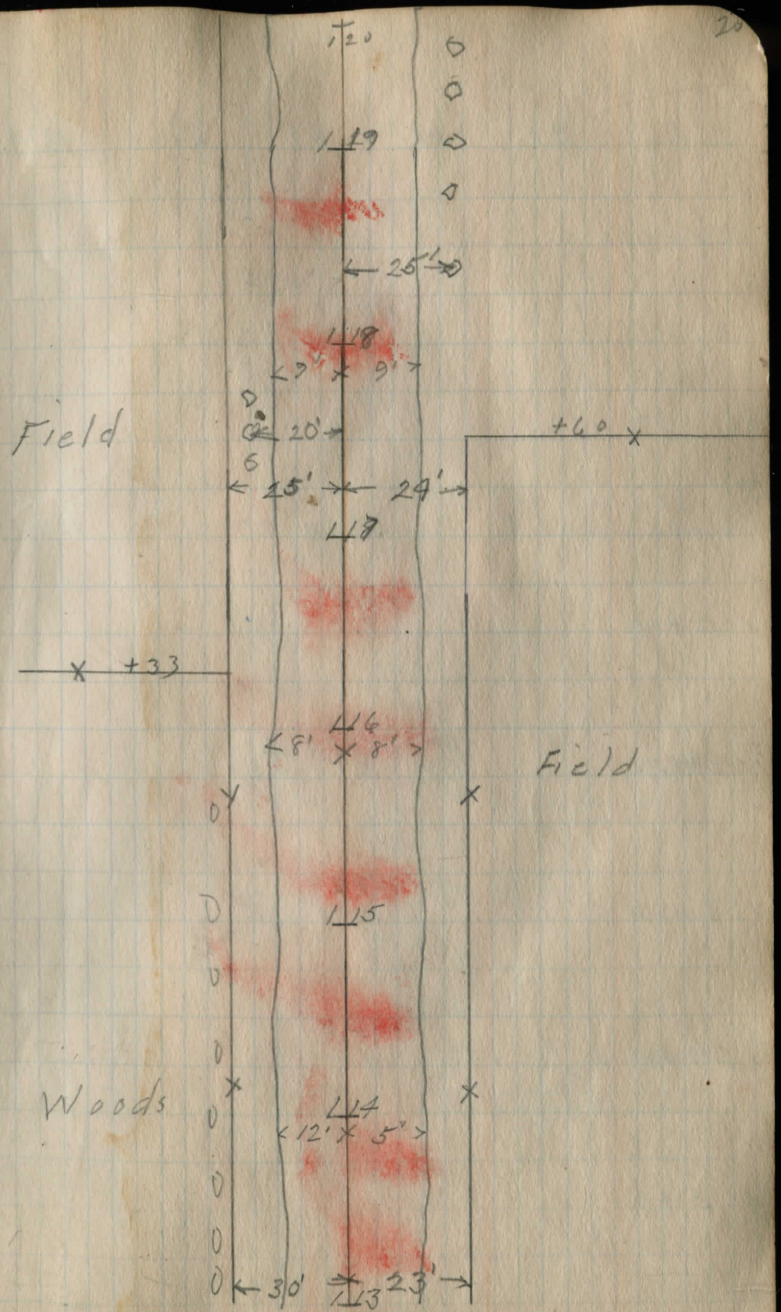


Undermined Conc. + Stone Culv to be used

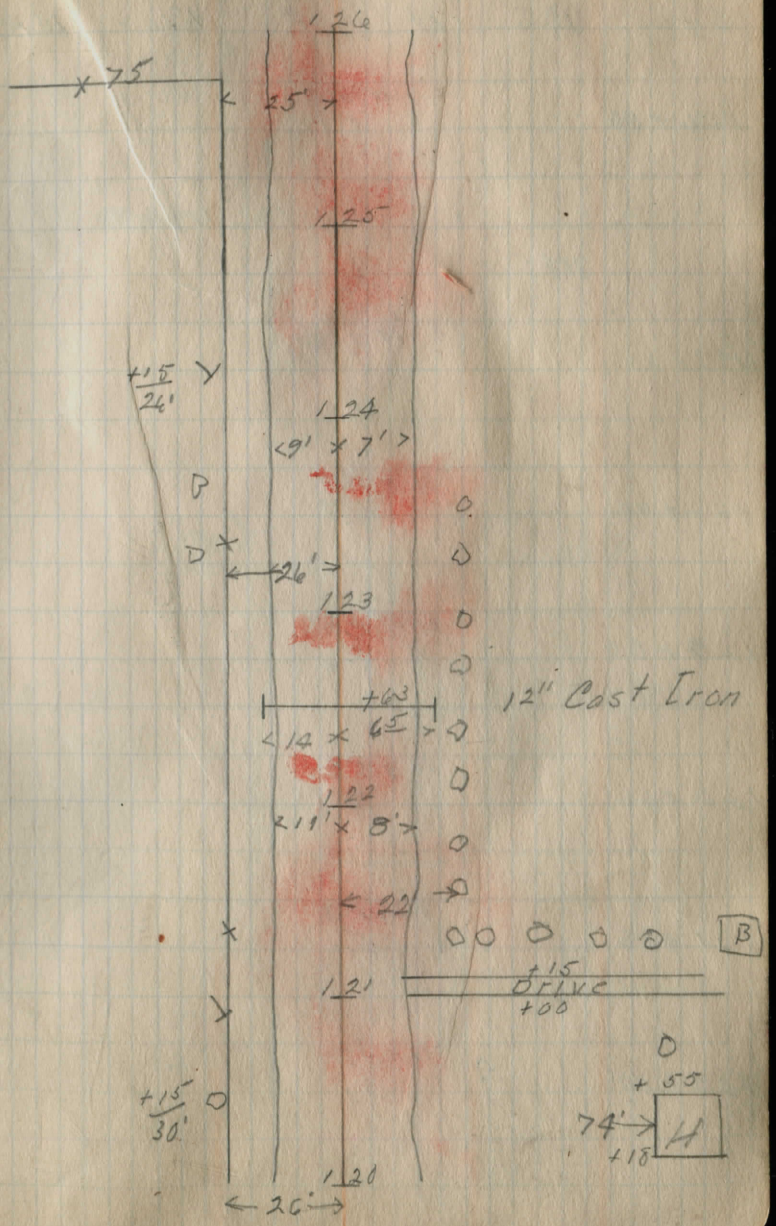
Sta	BS	HI	FS	Elev	BM
106+00		1181.4	5.9		
106+60		1185.0	2.3		
107+00		1185.7	1.4		
108+00		1184.3	3.0		
109+00		1182.4	4.9		
110+00		1181.0	6.3		
111+00		1179.9	7.4		
112+00		1179.3	8.0		



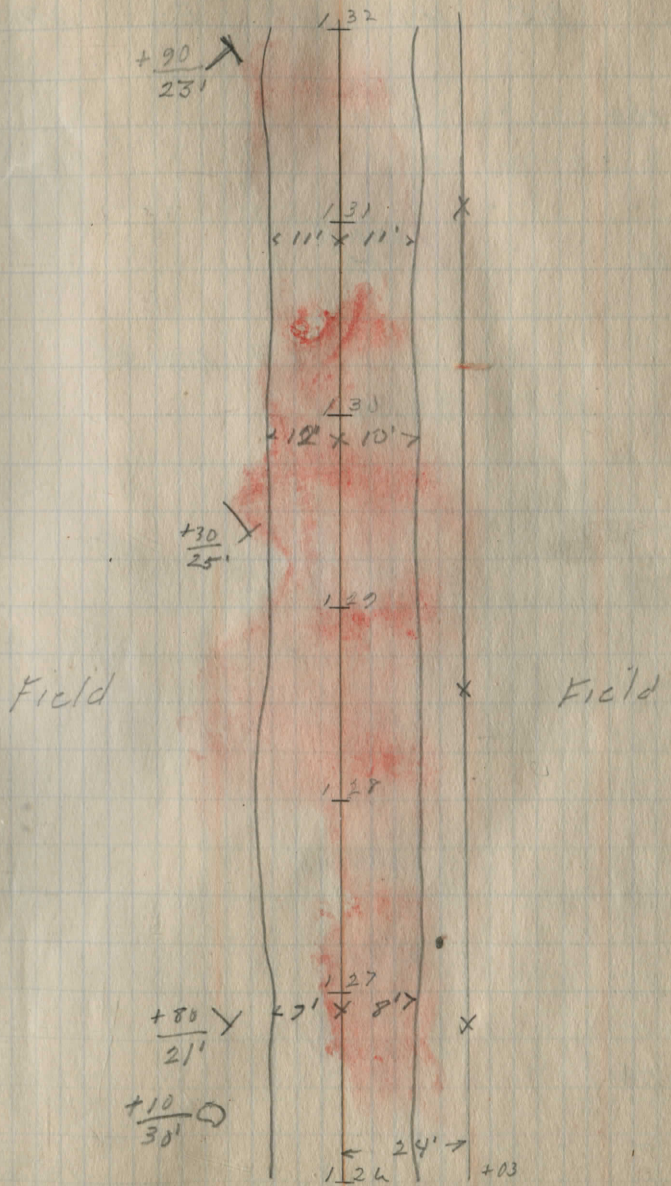
Sta	BS	HI	FS	Elev	BM
112+08 Culv	17 / 10.3	1179.3 8.0	7 / 10.3		
113+00		1179.6 8.3			
			7.63	1179.63	
	12.69	1192.32			
114+00		1178.8 13.5			
115+00		1179.3 13.0			
116+00		1180.3 12.0			
117+00		1181.3 11.0			
118+00		1182.6 9.7			
119+00		1184.6 7.7			



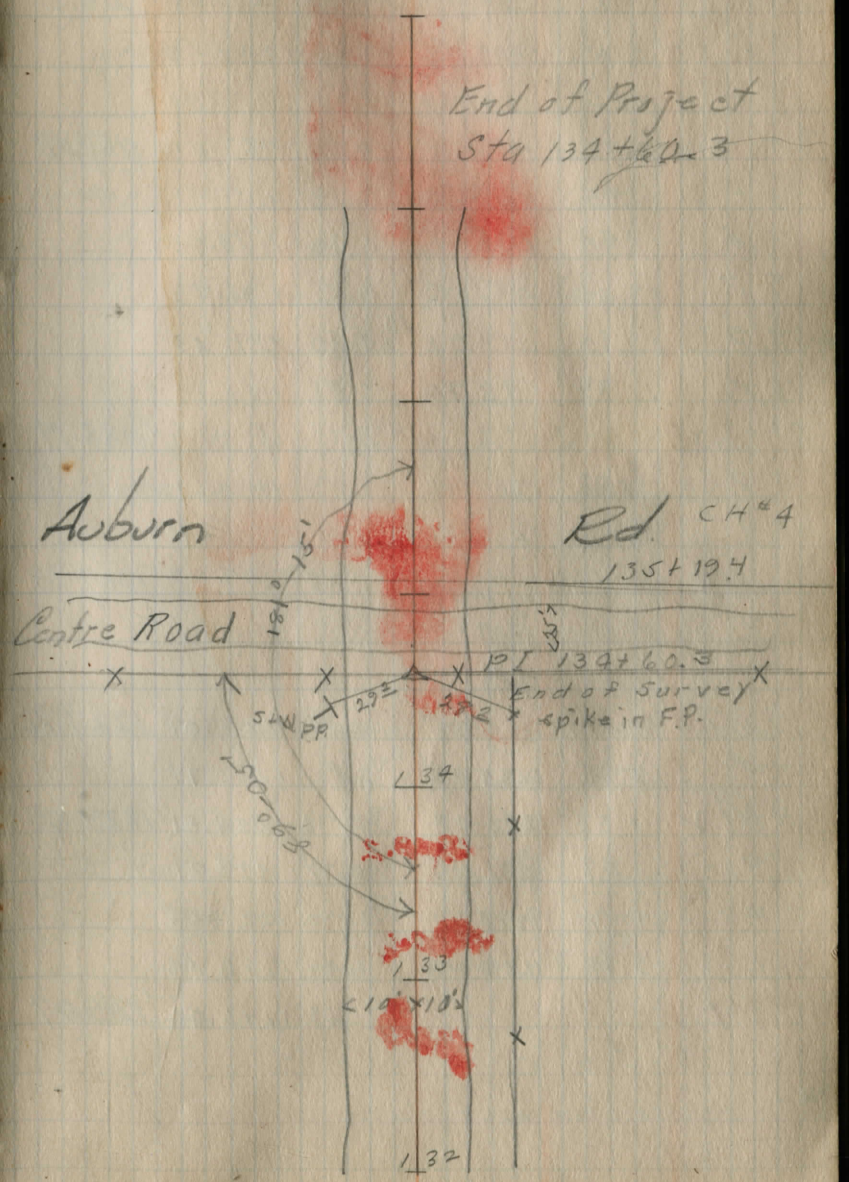
Sta	BS	HI	FS	Elev	BM
		1189.06			
120+00			3.3		
		1191.1			
120+75			1.2		
		1191.1			
121+00			1.2		
BM Sta Nail in Maple 121+20 22' Rt ℄			0.00	1192.32	
		1190.5			
122+00			1.8		
	14	1190.2	7		
122+63	3.4		2.1	3.2	
		1189.8			
123+00			2.5		
		1190.4			
124+00			1.9		
		1190.7			
125+00			1.6		



Sta	BS	HI	FS	Elev	BM
126+00		1191.2	1.1		
			1.33	1190.92	
	11.85	1202.84			
127+06		1191.9	10.9		
128+00		1193.0	9.8		
129+00		1194.2	8.6		
130+06		1195.7	7.1		
131+06		1197.2	5.6		
132+00		1198.7	4.1		



Sta	BS	HI	FS	Elev	BM
		1200.0			
133+00			2.8		
		1201.4			
134+00			1.4		
			1.64	1201.20	
	11.14	1212.34			
		1200.7			
		1200.7			
134+90	2 Road	200/8.5	100/8.3	600/7.6	200/5.8
					5.0
		1204.2			
135+00			8.1		
		1208.2			
136+00			4.1		
		1210.6			
136+75			1.7		
		1210.1			
137+00			2.2		
B.M. Sta. 135+70	Nail in pine 30' Lt. ℄		3.20		1209.14



LEVELS BELL ST.

	+	HI	−	E	Corrected E
B.M. Fd	1.11	1211.48	1.13	1210.37	1210.37
T.P.	0.70	1201.55	10.63	1200.85	
T.P.	4.55	1197.52	8.58	1192.97	
B.M. 6	0.10	1187.11	10.51	1187.01	1187.03
T.P.	8.95	1189.93	6.13	1180.98	
T.P.	7.45	1185.48	11.90	1178.03	
T.P.	13.00	1198.33	0.15	1185.33	
T.P.	0.80	1188.33	10.80	1187.53	
T.P.	10.88	1192.70	6.51	1181.82	
B.M. set 5			3.99	1188.71	1188.79
T.P.	11.82	1202.49	2.03	1190.67	
T.P.	8.73	1210.72	0.00	1202.49	
B.M. 4			2.95	1207.77	1207.78
T.P.	9.00	1219.34	0.38	1210.34	
T.P.	9.97	1227.47	1.84	1217.50	
B.M. 3	1.85	1224.92	4.40	1223.07	1223.12
TP	12.85	1235.59	2.18	1222.74	
B.M. 2	1.68	1226.49	10.78	1224.81	1225.72
T.P.	7.48	1233.25	0.72	1225.77	
T.P.	1.46	1223.41	11.30	1221.95	
T.P.	3.72	1220.18	6.95	1216.46	
B.M. 1			5.18	1215.00	1215.07

B.M.'s NUMBERED FROM WEST TO EAST

FROM AUBURN ROAD West to So. RUSSELL

Spk S.W. root 24" Pine ± 10 4' E of Auburn Rd N side of Bell

Bent over spk NW root most Wly Maple rear left west of Button Side N. Edge / rear W end 1st called W of Button

SPK NW ROOT 15" ELM 25' N OF ℄ WEST SIDE L. GORE lawn

SPK N. ROOT 20" MAPLE FOURTH MAPLE EAST L.W. FROM DRIVE RING also EAST OF CEI POLE 191500 E across road

Spk S root 30" So. Map S side road opposite W. Thomas drive - Brick house (opposite 576566) CEI pole

Spk NW root 20" Ash ± 250' E of W. Benbow's house S side rd

Spk SW root 40" Elm N side rd ± 100' E of end of pavt

1/16/50

	+	HI	−	El	
BM 1	10.80	1225.37		1215.07	
0+0			7.86	17.5	
1+0				16.3	
1+64				15.8	CULVERT
2+0				15.7	
0 – 100'				19.4	
0 – 280				23.7	
T.P.	12.43	1237.50	0.30	1225.07	
0-300				28.5	
0-400				32.4	
0-450				32.5	
0-500				31.2	
0-600				25.4	

E S 23

spk SW. root 40"

Sta 2+42 30' Lt Elm

7.86 9.30 9.10
16'S of P.I 35'S of P.I 60'

9.1 10.7
℄ 50'

13.3 13.0 13.2 13.0 9.6 12.6 11.0
200 150 100 N.F.L. ℄ S.F.L. 40'

9.7
℄

6.0
℄

2.2
℄

10' Rejt

9.0
℄

① 28 d-d
② 26 d-d

5.1

5.0 So Russ

6.3

12.1

	+	HI	−	Elev
BM 1	8.00	1223.07		1215.07
3+00				
4+00				
5+00				
6+00				
7+00				
8+00				
T.P.	10.66	1233.23	0.50	1222.57
9+00				
10+00				
11+00				
12+00				
13+00				
14+00				
15+00				
16+00				

E

5pk SW root 40" Elm 30' N of 2+42

7.0	16.1
6.4	16.7
5.7	17.4
4.9	18.2
3.3	19.8
1.8	21.3
9.9	23.3
7.9	25.3
6.1	27.1
5.0	28.2
4.0	29.2
3.2	30.0
4.3	28.9
6.1	27.1

1233.23 ✓

17+0				25.7 ✓	
TP	1.15	1226.76 ✓	7.6 ✓	1225.61 ✓	
~~18+0~~				25.7 ✓	
18 ~~19+0~~				23.7	
19 ~~20+0~~				22.5	
~~21+0~~ 20				22.2	
~~21+09~~ 20+09				22.1	Culvert
21 ~~22+0~~				21.7	
22 ~~23+0~~				22.1	
23 ~~24+0~~				22.9	
24 ~~25+0~~				23.9	
25 ~~26+0~~				25.0	
~~TP~~ BM 2	25.05 / 15.00 / 10.05 use	1.65	1225.11 ✓	(1125.12)	

see ok next pg:

N

S

7.5
E

1.1

3.1

4.8/30 4.6/17 6.0/13.6 5.0/11 4.3 4.8/9.5 6.2/14 4/23 3.5/30

4.6

9.5/100 8.1/NFL 4.7 7.81/SFL

5.1

4.7

3.9

2.9

1.8

Sta 24+81 25' Rt Spk NW root 20" Ash

check

B.M.	7.95	1222.95		1215.00
T.P.	10.00	1232.51	0.44	1222.51
T.P.	1.28	1226.87	6.92	1225.59
B.M.			1.81	1225.06
B.M.2	10.86	1235.98		1225.12
~~27+0~~	26			25.1
~~25+0~~	27			28.9
~~29+0~~	~~28~~			31.9
~~27+50~~	28+50			32.9
~~30+0~~	29			32.7
~~31+0~~	30			30.5
~~32+0~~	31			27.6
T.P.	0.11	1226.71	9.38	1226.60
~~33+0~~	32			25.2
~~34+0~~	33			23.5
~~35+0~~	34			22.6

	10.87
	7.1
	4.1
	3.1
	3.3
	5.5
	8.4
	1.5
	3.2
	4.1

		1226.71			
~~36+00~~	35			21.7	
~~37+00~~	36			21.0	
~~38+00~~	37			20.6	
~~39+00~~	38			20.4	
TP.	4.94	1225.~~35~~ .36	6.30	1220.41	
~~39+67~~	38+67			20.6	CULVERT
~~40+00~~	39			20.8	
~~41+00~~	40			20.8	
~~42+00~~	41			21.0	
~~43+00~~	42			21.2	
~~44+00~~	43		3.24	21.9	
BM 3			2.24	1223.11	(1223.12)
~~45+00~~	44			22.1	
TP	5.29	1227.55	3.10	1222.26	
~~46+00~~	45			22.2	
~~47+00~~	46			23.3	

N

S

5.0

5.7

6.1

6.3

7.0 Rt. 4.8 7.4 / 5, F.L. 7.4 / 100

5.0 / 30 5.7 / 20.5 7.3 / 15.5 5.3 / 12 4.6 5.3 / 10 6.2 / 13 5.4 / 17 5.9 / 30

4.6

4.4

4.2

3.5

Sta 42+98 25' Rt Spk Sroot 30" So. Map

3.3

5.3

4.2

		1227.55		
~~A8+0~~	47		23.5	4.0
~~49+0~~	48		21.7	5.8
~~50+0~~	49	Spt set out from	20.2	7.3
		I.P. = 50+00		
~~51+0~~	50	profile meas.	19.2	8.3
~~52+0~~	51		18.4	9.1
T.P	3.79	1221.62	9.2 1212	8.33
~~53+0~~	52		17.8	3.8
~~54+0~~	53		17.3	4.3
~~55+0~~	54		16.7	4.9
~~56+0~~	55		16.0	5.6
~~57+0~~	56		15.3	6.3
~~58+0~~	57		14.6	7.0
T.P.	2.10	1217.14	7.38 1214.24	
~~59+0~~	58		13.9	3.2
~~60+0~~	59		13.6	3.5

3.7/30 3.8/17 5.4/14.5 4.3/12 4.1/9.5 5.2/12 4.2/13 4.2/30

						N	S
		1217.14					
~~61+0~~	60			13.1		4.0	
~~62+0~~	61			11.7		5.4	
~~63+0~~	62			09.7		7.4	
~~64+0~~	63			07.3		9.8	
~~65+0~~	64			06.5		10.6	
T.P.	3.14	~~1211.90~~	10.38	1206.76			
~~65+15~~	64+15	1209.94		06.4	Culvert	8.2 / 100 — 7.20 NFL	3.5 — 7.25 SFL
~~66+0~~	65			05.7		4.2	
~~67+0~~	66			05.7		4.2	
BM 4			2.16	1207.74	(1207.78)	66+27 24' Rt Spk N root 20" Maple	
~~68+0~~	67			04.5		5.4	
~~69+0~~	68			02.2		7.7	
~~70+0~~	69			1200.2		9.7	
T.P			10.38	1199.16		Hob NW ℄ intersection	

	+	HI	−	E
T.P.	7.37	1206.53		1199.16
69+65.9				1200.1
70×65.9 = Mun Rd				
1+0				
2+0				
1+53				
				COLVERT
3+0				
4+0				
5+0				
6+0				
T.P.	1.65	1200.81		1199.16
~~7+0~~	7+0			98.2
7~~3~~+23				98.5
7~~4~~+0				98.9
+50				99.0
7~~5~~+0				97.6
75+0				92.8
76+0				90.0

426

S

TH 147 G
℄
North

98.1 8.4

11.3 WFL 8.3 11.7 EFL

8.9

97.6

℄

6.4
℄
3.1
1.2
0.6
0.3
1.4

TH 147 E
South

CH 410 SEC E.

2.6

7.1 / 1.90 4.6 WFL 2.3 4.5 FL

1.9
1.8
3.2
8.0
10.8

1200.81

77+0			88.5	
T.P.	5.48	1193.31	12.98	1187.83
~~80+0~~ 79		1193.25		87.9
~~81+0~~ 81				88.4
82+50				88.6
BM 5			4.46	1188.85 (1188.79)
83+50				85.6
84+0				83.4
85+0				82.2
85+82				Culvert
T.P.	4.38	1186.18	11.45	1181.80
85+82				81.8
87+0				81.1
89 ~~90+0~~				82.2
91 ~~92+0~~				84.9

Red: corrected Sta

℄

N								S
				12.3				
6.2 (30)	6.3 (15)	7.2 (14)	6.2 (11)	5.4	6.0 (10.5)	7.1 (13)	6.5 (17)	5.3 (30)
				4.9				
				4.7				
Sta. 83+09 24' Lt								
				7.6				
				9.8				
				11.0				
				11.5→81.7				
9.3 (100)	1.7 (10 Ft.)	4.4	7.6 (5 Ft.)					
				5.1				
				4.0				
				1.3				

1186.18

T.P	13.05	1199.23	0+0	1186.18
92+0				86.7
93+0				90.1
94+0				91.9
95+0				96.6
+54 = I.P.				
96+0				94.7
97+0				91.9
T.P.	0.37	1186.71	12.89	1186.34
~~100+0~~ 99				85.0
101+0				79.6
102+20				77.7
T.P.	12.24	1188.57	10.38	1176.33

15 cubic

N 5

12.5
9.1
4.3
2.6
9.5
7.3

1.7 1.8 3.5 2.3 1.7 2.5 2.9 2.5 0.3
30 16 17.5 10 11.5 13 15.5 25

7.1

74.7 74.8
RONO 12.0 9.0 11.9
30'N NFL SFL

1.03+60 to 10+40
H₂O over rod 1/16/50
build up 1 min.

		1188.57							
				77.2			11.4		
103+0									
104+0				77.7			10.7		
105+0				79.6			9.0		
106+0				82.9			5.7		
107+0				86.8			1.8		
108+0				86.0			2.6		
109				84.0			4.6		
111+0				81.8			6.8		
T.P.	3.65	1185.30	6.92	1181.65					
112+11			From 11,5	80.7	CULVERT	(NEW CULV JULY 1950)	77.7 7.6 N.F.L.	4.6	76.7 8.6 OF E
113+0				80.9			4.9		
	114+70 TO 115-30 WASHOUT								
114+0				80.3			5.0		
115+0				80.9			4.4		
117+0				82.8			2.5		

#119 STATION FROM N.E. CULVERT N.E.

1165.30

T P.	12.48	~~1199.17~~	0.61	1184.69	
B.M. 6		1197.23	10.20	1186.97	(1187.03)
~~1+070~~	119			86.2	
120+0				90.4	
121+0				92.7	
122+0				92.2	
123+0				92.1	
123+66				92.1	CULVERT
125+0				92.6	
T P.	6.39	1199.30	4.32	1192.91	
127+0				93.9	
129 ~~1+070~~				96.0	
131+00				98.8	
T P.	13.02	1211.44	0.88	1198.42	
133+0				101.7	

5

1184.75 25' RT

12.4 / 30	12.2 / 19	12.5 / 17.5	11.7 / 11	11.0	11.8 / 10.5	12.3 / 13	12. / 17	11 / 19	9.4 / 24.50
				6.8					
				4.5					
				5.0					
				5.1					
8.7 / 100 N.Wly		9.1 / NFL.		5.1	7.5 / SFL.				
				4.6					
				5.4					
				3.3					
				0.5					
				9.7					

1211.44

03.2

134+0

+94.8 = 1P & #4 #10

B.M. 1.09 1210.35 (1210.37)

134+94.8 06.3

B.M. 5.62 1215.99 1210.37

136+0 08.7

137+0 11.7

138+0 08.2

139

~~140+0~~ 05.0

T.P. 0.20 1204.05 12.14 1203.85

141+0 1200.8

℄

8.2

North CH #4 South CH #4

℄			℄	
05.4	6.0	200	2.7	08.7
		300	1.6	09.8
05.4	6.0	400	2.4	08.8
04.7	6.7	500	3.4	08.0

CH. #10

7.3

4.3

7.8

9.8/30 9.8/23 17.4/14 12.5/12.5 11.4/10 11.0 11.5/10 12.7/12.5 11.4/15 10.6/30

3.2

		↓ 120406			
143+0				1198.0	6.0
144+0				96.4	7.6
145+0				93.6	10.4
T.P.	0.32	1192.70	11.67	1192.38	
146+0				90.3	2.4
147+0				88.4	4.3
148+0				87.4	5.3
149 150+0				88.6	4.1
+21.5	WEDGE SHOT B			89.4	9.8/WFL 3.31 9.7/SFL
151+0				88.3	4.4
151+0				88.8	3.9
T.P.	13.18	1204.73	1.15	1191.55	
153+0				92.8	11.9
154+0				95.5	9.2
155+0				1199.9	4.8
156+0				1203.9	08

		1204.43			
T P.	12.50	1216.98	0.25	1204.48	
157+0				07.5	
B M. SET			7.05	1209.93	
158+0				10.4	
159 160+0				14.7	
160+0				16.5	
161+0				15.5	
162+0				14.3	
T P.	5.90	1220.02	2.66	1214.32	
162+78				14.0	CULVERT
163+0				14.0	
165+0				16.2	
167+0				14.7	

N

9.5

30" SMAG S. ROOT W & E MAX X 157 ± 20 40' Lt

6.6

23

0.5

0.6/30 1.4/17 2.3/12 1.8/9 1.5 2.2/7 2.2/10.5 3.0/30

2.7

8.0 NPL 6.0 8.7 SPL 9.0 FL. FLOW DRAIN 30' S WLY

6.0 14.0

3.8 16.2

5.3 14.7

	20' East of Bnch	1220.02		1214.32	
167+53	W. Breast			12.7	Culvert
169 ~~170~~					
T.P.	9.06	1224.55	4:53	1215.49	
171+0					
172+30					
173+0					
175+0					
177+0	✓				
BM	8.67	1224.25	8.97	1215.58	(W.M. 1215.63)
179+24		US 4429	W. marks 4427		Culvert
				14.7 ✓	
~~179+0~~ 180				15.0 ✓	
181+0				17.3 ✓	
182+0				19.9 ✓	
183+0				19.8 ✓	

	7.4 N.P.L.	5.3	7.5 S.F.L.	7.5 F.L. of E 50' S.E.ly
		4.7	15.3 ✓	
		6.8	17.8 ✓	
		7.9	21.7 ✓	
		3.4	21.2 ✓	
		7.2	17.4 ✓	
		9.2	15.4 ✓	
179 →		10.0	14.6 ✓	

200'

HEXN hdw / culv't

100'

	12.8 100	12.6 N.P.L.	9.5	12.5 S.F.L.					
			9.3						
	FLs as read on muck Floor = ± 1' lower								
	3.5 28	5.3 15	8.3 11.	7.5 9.5	7.0	7.7 9.6	8.3 11.5	6.8 13.5	5.6 25	7.2 30
					4.4				
					4.5				

		1224.25		1215,58
184+0				
185+0				
T.P.	12.55	1236.41	0,39	1223.86
186+0				
187+0				
188+0				
T.P.	13,15	1249.36	0,20	1236.21
189+0				
T.P.	12,23	1261.36	0.23	1349.13
~~187+0~~ 190				
T.P.	11.55	1272.55	0,36	1361,00
191+0				
192+0				
192+50				
193+0				
194+0				
195+0				

4.0	20.3 ✓
2.5	21.8 ✓
11.8	24.6 ✓
7.6	28.8 ✓
0.5	35.9 ✓
4.1	45.3 ✓
7.0	54.3 ✓
10.2	62.4 ✓
4.5	68.0 ✓
3.3	69.2 ✓
3.7	68.9 ✓
6.2	66.3 ✓
8.6	64.0 ✓

		1372.55			
BM set	0.28	1360.74	12.09	1360.46	~~194+38~~ 195+38
197+00					
199+00					
T.P.	0.64	1348.42	12.96	1347.78	
201+00				41.9 ✓	
?					
203+00					
T.P.			11.00	1337.42	

196+34 35' Rt

NE Rod 20" Maple Dent Spot S side Rd

500' E of Rice

			3.3				57.4 ✓
			10.3				50.4 ✓
5.5	4.6	7.7	7.9	6.5	6.9	7.6	3.0
30	17	10.5	8		8.5	11	30
			10.9				37.5 ✓

State 17' NE of 203+00

Check for error in Station

BM		1221.58	6.58	1215.0	
1				1216.18	(16.2)
2				1215.58	(15.6)
3				1215.98	(16.0)
4				1216.48	(16.6)
5				1217.38	(17.3)
6				1219.08	
7				1219.08	
8				1221.18	
T.P.	11.22	1234 65	0.15	1221.43	
9				1223.35	23.3
10				1225.25	25.3
11				1227.05	27.1

ing

54
60
56
51
42
35
1.9
0.4
93
74
56

		1232.65		1221.43			
12				1228.15	28.2		4.5
13				1229.25	29.2		3.4
14				30.0	30.0		2.7
15				28.8	28.9		3.8
BM.			1.34	1231.31		14+80 Rod Set NE RT	Elev
T.P.	1.93	1230.78	3.80	1228.85			
16				1227.08	27.1		3.7
17				1225.58	25.7		5.2
18				1223.48	(25.6)		7.3
19				1222.38	(23.6)		8.4
20				1221.98	(22.4)		8.8

Culvert = 20 + 07

STATIONS HEREON CORRECT in Red

TP.		1341.71	4.29	1337.42				
203+77	6.52	6.87			Culvert			
204+0							5.3	36.4 ✓
205+0							5.5	36.2 ✓
206+0							4.2	37.5 ✓
207+0							2.3	39.4 ✓
TP.	12.59	1353.90	0.40	1341.31				
208+0							10.5	43.4 ✓
209+0							5.9	48.0 ✓
210 ~~207+0~~							3.8	50.1 ✓
211+0							1.7	52.2 ✓
T.P.	3.31	~~1351.12~~	0.90	1353.81				
212+0		1256 31 ✓		1253 0			2.2	54.1 ✓
213+0							2.3	54.0 ✓
214+0							8.3	48.0 ✓

5 Pk 30' for P. near Big Windy

N

36.6 30.5

11.0 5.1 11.2 16.7
M.F.L. S.F.L. F.L. Pipe C&E

		1357.12 56.31		1353.81	N									
T.P. 215+0	0.80	~~1345.24~~ 1244.43	12.68	~~1344.44~~ 1243.63		5.9	38.5 ✓							
T.P. 216+0	0.20	~~1332.38~~ 1231.75	12.88	~~1332.36~~ 1231.55		2.0	29.7 ✓							
217+0						9.2	22.5 ✓							
T.P. 218+0	1.10	~~1330.55~~ 1219.92	12.93	~~1329.45~~ 1218.82		3.1	16.8 ✓							
219+0 TBM	1.23	~~1314.86~~ 1214.23	6.92	~~1313.63~~ 1213.00		8.1	11.8 ✓							
~~220~~ 221					Spk S, Root 22' Ash 10' E of Post Drive	11.2	03.0 ✓							
T.P. 223+0	0.77	~~1303.25~~ 1202.62	12.38	~~1302.48~~ 1201.85		6.3/30	6.7/14	7.6/11	7.9/9	6.4	6.8/9	7.9/11	6.1/16	5.7/30	96.2 ✓
225+0						12.3	90.3 ✓							
T.P. 227+0	2.34	~~1297.99~~ 1192.36	12.60	~~1290.65~~ 1190.02		7.3	85.1 ✓							
229+0						11.6	80.7 ✓							
T.P. ~~228~~ 231	8.05	~~1198~~ 1188.21	.84 12.20	~~1190~~ .79 1180.16		10.3	77.9 ✓							
~~2324~~ 2324 53		US 9758	W.M 9753			14.3 NEL	11.5 TOEHN	11.5	11.5 STOPH	15.1 3 FT.	15.3 100			76.7 ✓

1188.21

233+0

234+0

235+0

236+0

237+0

238+10

239+0 8.44 1292.62 4.66 1284.18

TP 8.44 1292.62 4.66 1284.18

Z 31+13 1191.99 ✓ 1183.55 Correct

240+13

~~239+0~~ 241

~~240+25~~ 242+25

~~240+0~~ 243+0

B.M 3.77 J.M. ~~1188.22~~ (W.M. 1188.22)

240+15 1 2 5R 44

243+18

N

11.6	76.6 ✓
10.6	77.6 ✓
7.5	80.7 ✓
4.2	84.0 ✓
3.0	85.2 ✓
3.6	84.6 ✓
4.3	83.9 ✓
9.9 NFL 8.5	10.6 SFL 11.9 50 83.4 ✓
8.0	84.0 ✓
7.4	84.5 ✓
10.3	81.6
10.59	81.4

?

1191.99

				84.7
T.P. #1			5.75	1186.24
T.P. #2			11.15	1180.84
T.P. #1	2.21	1188.45		1186.24
Profile 44				
TP #2	0.60	1181.44		1180.84
TP	0.72	1169.16	13.0	1168.44
BM	7.90	1223.48		1215.58
178			9.0	14.5
176			8.1	15.4
174			6.1	17.4
BM	8.93	224.51		1215.58
179				(15.0)
180			7.2	17.3 (17.3)
181			—	— (19.9)
182			4.8	19.7 (19.8)
183				(20.3)

7.3 100' N of intersect #44

5.75 NE ⊙ Bottom Step

T.P. 11.15 NE ⊙ Concrete Monument

NE bottom step

78.5 80.8 83.0 85.0

10.0 7.7 6.5 3.5

500 400 300 200 ℄

north

69.7 75.7

11.7 5.7

200 100 South

54.5 56.1

up South 58.5 63.9

14.7 14.1 10.7 5.3

600 500 400 300

200 Error in Sta

24.51

184			2.7	21.8	(21.8)
T.P.	12.73	36.81	0.43	24.08	
186			7.9	28.9	28.8
T.P	12.61	49.04	0.38	36.43	
188			3.7	45.3	(45.3)
T.P.	11.72	60.48	0.28	48.76	
T.P. 190	11.20	71.59	0.09 / 9.2	60.39 / 62.7	(62.4)
192			2.8	68.8	(68.9)
194			7.7	63.9	(64.0)
BM	0.43	60.87	11.15	60.44	
196			3.4	57.5	57.4
198			10.4	50.5	50.4
T.P.	0.35	48.16	13.06	47.81	
200			6.2	41.9	(42.0)
201			9.0	39.2	(37.5)
202			10.6	37.6	
T.P.			10.74	37.42	

NPSD
at m c Stafford 200'

± 400' E of Mumm 190'

Typical Sect Mumm South
4' gravel 14' pave
22' d to d 1' berm

Mumm North
14' pave 2' berm
22' d to d gravel
hill W of Coates 190'
No interference
hill ± 800' E of Coates
just W of Button of Arching line = 170' 8' bank on N
no bank South

P.I. on Corp line 0+02.75 : 22' to S pvt edge
50 W of P.I = 11' " " "
100' " " " = 7' " " "
150' " " " = 5' " " & N

P.I 22.2 N to N edge pavt

4th intersect Make turnout ext's both 14'

Sta 22+0	1"	5"	℄		5"	1"
	11'	9'	10"		7'	8'

North South

14+0	2"	4"	9"		4"	1"
	11'	9.5'			7'	8'

42+0	3"	7"	9"		8"	4"
	10'	9'	℄		9'	10'

62	1"	2"	5"		6"	1"
	11'	10'			7'	8'

Munn Rd Turnout Ext

SE & SW 10'
NW 19'
NE 23'

74+0	0"	1"	2"	3"	2"	1"	1/2"
	9'	7'	6'		8'	11	13'

96	0"	2" sandy	5"		1"	0"
	9'	7'			8'	10'

114+0	some gravel w/ 6" clay		6"	9"		8"
	9'	7'				9'

Turnout Ext. at No 4

SW 11' SE 14'
NE 14' NW 14'

			℄ DSN	2 typical See #4		
	2' berms		18'	2' berms		

140	3" fine sand NG	10" sand		8"	2"	0"
	10'	8'			7'	9'

160	5" sand	8" sand	most sand		7"	5" sand
	9'	7'	10"		7'	8.5

NBSD 260' 160+0
11 150' 135+0

180	0"	4" mottled clay			4" with lots of clay	0"
	9'	8'		9"	8'	10'

192+0 ± 180' NPSD

213 160' NPSD
192+0 - 193+0 Mud hole
no gravel

202+0 1" 6" 6" 10" 8" 1"
7' 5' 8' 10' 11

all fine with sandy clay

220 4" sand 7" 7" 7" 2"
10' 8' 5' 6'

238 4" sand 8" 12" 6" sandy loam 2" Sand
10 8' 6' 8'

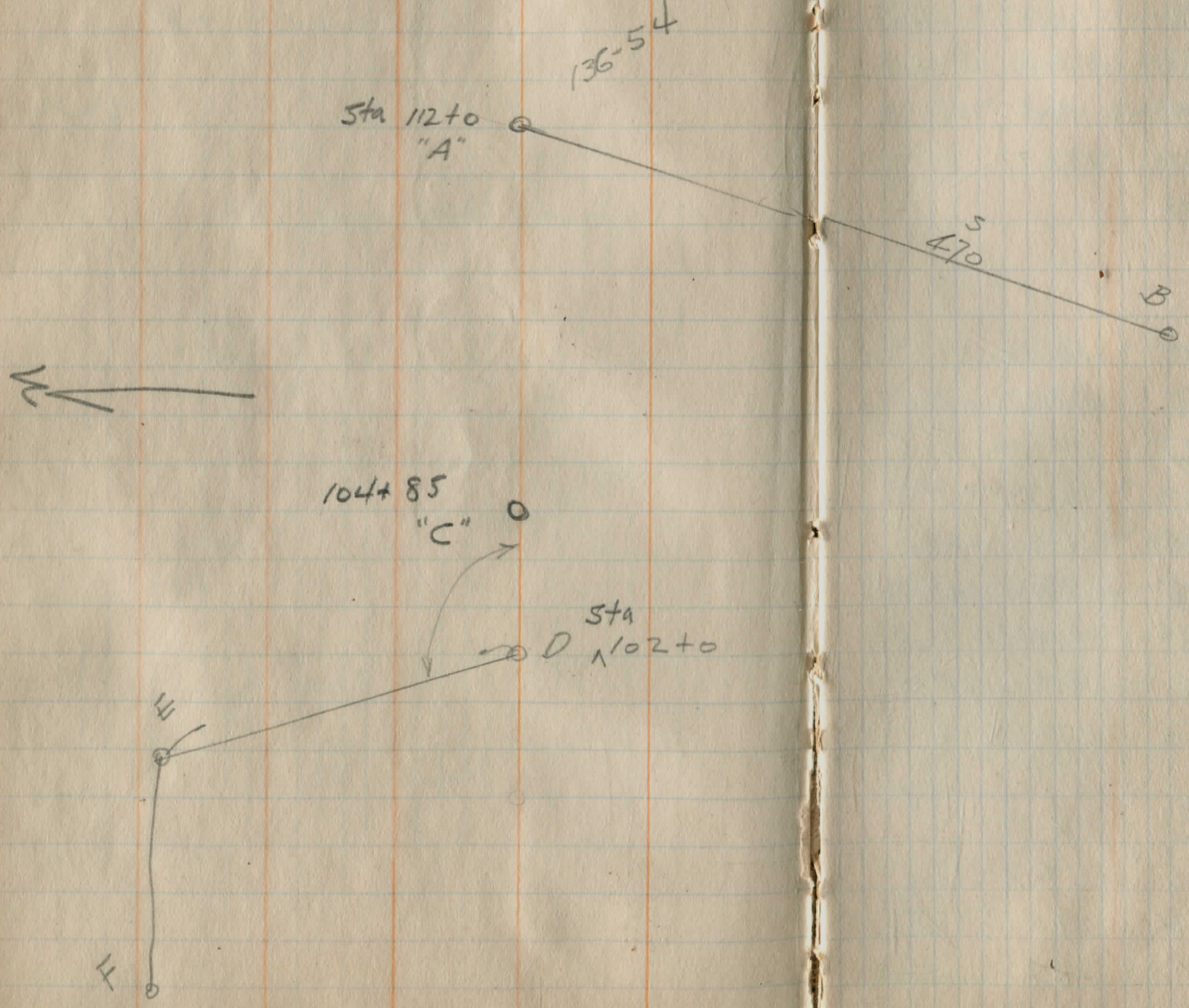
Zyp Sect UU

18' pract
30' 6 to 6

BUTTON - FROHRING

± Feb. 1950 ℄

SWAMP HOLES BELL ST



Set on BS		Lt or Rt	Stadia	Rod	
T.P.	5.11	1186.11		1181.00	
"A"	℄ east	335-30	136'	7.8	78.3
		65-20	38'	8.8	77.3
		77-17	85'	7.8	78.3
		83-26	254'	9.4	76.7
TP	5.90	1186.67	5.34	1180.77	
		136-54	470		
Set on B-BS. on A.					
		46-10	327'	8.9	77.8
		46-10	350'	7.2	79.5
		" "	313'	"	79.5
		66-16	320	8.7	78.0
		61-24	280	7.0	79.7
		126-40	81	8.8	77.9
		221-04	223'	8.9	77.8
		227-25	298	8.9	77.8
T.P.			9.0	1177.67	
Set on C ℄ east					
T.P.	8.30	1184.63	290'	1176.33	
T.P.		77-13	6.6	1178.0	
		79-03	234'	7.9	76.7
		136-10	87'	8.8	75.8
				9.8	74.8

H. Holwl near Wend

In swamp N Side Rd H_2O 6/10 deep 25' E 200' N.E.

N.E end R.R. Tile H_2O 6.7 deep 11' long 24"d

H_2O 6/10 Good Chan North. Spread to South & Underbrush

H_2O 12" S. End Brush, Swamp Narrow to 6' Chan l.

⇒ pt in Chan l H_2O 12"

Top E. Bank

" W. "

⇒ wly 8/10 H_2O Sm Dr. ditch from S.E.

Fence ⇄ W & N

℄ Chan l at P.L. But-From 7/10 H_2O 75' wide Brush West

Chan l Wly thru 100' cut Hi Banks H_2O 7/10

" W. end Hi Banks H_2O 5/10

Chan l ⇒'s N toward Rd.

Chan l, Swampy both sides

End Swamp at S Side Cee, 8' wide Chan l. West 4' on S 6' on N

Cul inlet P.L.

Seton	B.S.	L to Rt	Stada	Rod		
T.P.	6.97	1183.30	6.97	1176.33		
D	℄ East					
		284-33	40'	8.5	74.8	Begin Chan'l
		229-50	213	9.2	74.1	Where outlet of Pond should start H_2O 1.1
		223-10	426'			
TP,	10.85	1186.37	7.78	75.52		
E	D					
		283-10	63'	13.0	73.4	Chan'l, Hell Lot Tag Willier Sly H_2O 1.2
		185-30	70'	13.1	73.3	Inlet Fl. Cem. Culv 2x2.8 ft Stone Box x 12'
				9.1		& Cem Drive on Culvert
		129-25	206.	14.1	72.2	Chan'l of Q'flo small dam rear Coates House
		139-30	270	15.4		Chan'l
T.P. & trav	(F)	136-57	317	10.70	1175.67	
T.P.	5.10	80.79		1175.69		
Sd F	E					
		261-10	68'	11.0	69.8	Chan'l
		250-28	166'	11.6	69.2	"

BELL STREET BASE TESTS JUNE 5TH 1950
TEMPLE & MAYNARD

N

E

S

2+00

10+00

20+00

30+00

40+00

50+00

66+00

MUNN Rd ℄

70+00

90+00

90+00

100+00

110+00

120+00

130+00

6"

9'
6" STONE & SAND

9'
10" SAND ST

4" 9'
5" STONE

9'
7"

9'
6" STONE & SAND

8" STONE SAND HARD LINE HOLE

1' N of N track ℄ 9'
S Track of Turn out 9"

9' S of N DITCH

SAME 10' S of ℄
7" → STONE & SAND HARD ↘ LINE HOLE

DITCH 2' 9' 9" ↑ 9' Edy - Ditch
3" GRAVEL ON SAND 6" SAND

DITCH 2' 9'
6" SAND CLAY

7" PITCH 10'
23' N DITCH 9'
7" ST & SAND

4" 10' S of Travel ℄ 8'
SAND STONE 5TH Ditch

6-22-50 + SECS BELL ST #10 SEC C

	+	H.I.	−	Elv	Corrected Elv
B.M.			7.22	~~1186.97~~	1187.03
TP	8.23	1195.20	2.62	~~1192.58~~	1192.64
TP.	4.66	1197.24	2.67	~~1194.57~~	1194.63
TP.	8.82	1203.39	0.40	~~1202.99~~	1203.05
TP.	12.50	1215.55	✓		

136+00

137+00

138+00

139+00

TP. 2.74 1207.08 11.21 1204.34

N

E

S

SPK NW RT 28" MAPLE (TRY) WEST BUTTON DRIVE

06.1 1206.3 06.6

9.4 / 10 — 9.22 — 8.93 / 30 — E to K

09.5 07.5 08.0 08.5 08.9 07.5 06.8 09.5 09.5

BM TREE — SAME OUT 6.0/17 — 8.0/10 — 7.5/6 — 7.0 — 7.6/10 — 8.0/14 — 8.7/15.5 — 6.0/22 — 6.0/30

DITCH — DITCH

E 30' +20

E 30' +53

+77 ← 29' → CCI

12.8 12.7 11.4 11.8 11.3 10.7 12.2 11.6

TREE 28' — 2.8/30 — 2.9/17 — 4.2/10' — 3.9 — 4.3/10 — 4.9/13 DITCH — 3.4/19 — 4.0/30 — MAY

Milanich — DRIVE — +14 — +25

OBT 24' +42

11.1 07.3 07.7 08.1 07.7 07.3 10.0 9.6

LEVEL OUT GARDEN — 4.5/17 — 8.3/12 DITCH — 7.9/10 — 7.4 — 7.9/10 — 8.3/11.5 — 5.6/18 — 6.0/30 — MAY

+28 DITCH CCI

OBT 25' +50

06.7

SAME OUT WHEAT — 5.9/25 — 03.9 — 11.7/13 — 04.7 — 10.9/10 — 05.0 — 10.5 — 04.5 — 11.1/16 — 03.8 — 11.9/12 DITCH — 05.0 — 10.6/17 — 05.4 — 10.2/30

1207.08 ✓

139+ + HI — ELV

140+00

BM 1209.93

9.00 1218.93

157+00

158+00

159

N E S 56

+48 27' ⊙

+78 28.5' CCI

07.8

LEVEL 4.1 4.6 5.8 4.5 4.3 4.5 5.5 4.7 3.9
WW287 25 17 13 10 9 12 16 30
DITCH DITCH

140+10 OBTE25 →

Spk 30' STAGBARK WOLFTRAX DRIVE 157+ ±20

154+45 = E Edge Simpsons Drive
07.5

11.1 11.3 12.3 11.4 11.5 ±12. 10.3 9.5
30 16 14 7 9 15 25

WOLF DRIVE +2.1
+33
OBT. 25' +50 24' PINE ⊙

10.3
6.7 8.4 9.2 8.6 9.4 9.6 9.5
30 14 10 10' 16 30

+58 — 27' — CCI.

MAPLE — 31' — +98

14.5
−1 0.0 2.5 1.7 4.4 4.4 5.0 5.6 6.2 Max
30 27 19 11 7 9 15 30

+ N 1218.93 — EL

159+

160+00

T.P. 4.10 1219.54 3.49 1215.44

161+00

162+00

CULVERT-1 479

163+00

164+00

N S

OBT - 24' - 484

450

HAWK DRIVE

474

16.5

±1.5/30 3.3/13 3.0/12 3.1/11 2.7/7 2.4 3.1/9 4.5/18 5.1/30 MAY

15.4

±3.2/30 4.6/14 4.9/11 4.1 4.6/8 5.0/13 4.7/15 5.6/30 MAY

Corn

14.2

EASY UP OUT 1.9/26 5.6/14 5.7/11 5.3 6.1/10 6.5/12 5.8/30

411

28'

444

475

Corn

14.0

EASY UP 5.5/25 7.5/F.G 12 5.7/10 5.5 6.0/8 7.9/11 F.L 6.9/17 6.6/30 MAY

14.1

4.9/29 6.1/13 5.7/11 5.4 6.0/8 6.6/14 6.6/30 MAY

443

28'

475

Corn

482

15.0

Poison Ivy 5.3/11 4.5 5.5/10 4.7/17 4.0/30 MAY

	+	H.I.	−	Elv
B.M.				1215.58 ✓
T.P.	9.07	1224.65 ✓	0.36	1224.29 ✓
T.P.	11.71	1236.00 ✓		
186+00				
188+00				
T.P.	12.32	1248.14 ✓	0.18	1235.82 ✓
188+00				
B.M.			6.86	1241.28 ✓
	11.88	1253.16 ✓		
189+00				
T.P.	13.04	1266.06 ✓	0.14	1253.02 ✓
190+00				

N ℄ S.

NE ▷ NW with W of George's 179 ± 25

24.6

+3' down at 30' 12.1/15 12.9/13.5 12.4/12 11.42 11.98/10 12.7/13 10.7/25 UP Sharp to CFIE

36.0

1.9/13 .90/11 0.00 .80/10 1.4/12

pace ditch

38.3 36.0 36.1 40.6

Slope North 9.8/23 12.1/15 12.0/14 7.5/25

+70 30' cE

26' +34

30' +54

40' +91

26' +93 +93

45.3

43/40 3.6/30 3.5/21 9.1/11 8.4/9 7.9 8.2/9 8.7/11 3.5/25 4.2/30 3.1/40 UP ±4'

±N-O-N

30' +15

+96 30' cE

54.3

Down easy 8.5/40 8.5/30 9.4/18 12.8/10 12.4/8 11.8 12.4/11 12.9/13 10.8/18 9.8/30 10.8/40

ditch ± S-on

		1266.06 ✓		
	+	H.I.	-	Elev
190				
191+00				
TP.	9.38	1275.07 ✓	0.37	1265.69 ✓
192+00				
192+50				
193+00				
193+50				DRIVE
194+00				
TP	1.34	1270.73 ✓	5.68	1269.39 ✓

N S

59

O.B.T. 22 +65

@ 28 +94

61.3

0.8/40 0.7/30 0.7/20 4.8/10 4.7/8 4.8 4.4/12 5.1/15 3.7/19 4.5/30 6.1/40

π-o-w

@ 28 +8

@ 23' +33

+70 30' CCI

68.0

2.9/40 3.3/30 4.5/21 5.2/10 8.0/9 7.1 7.8/13 8.3/15 7.7/20 11.7/40

(LAWN) DITCH π-o-w

@ T 21 +20

69.2

House UP 2.4/40 3.6/30 3.2/20 6.5/7 5.9 6.7/16 4.6/19 4.6/22 10.7/32 10.5/40 UP

LAWN π-o-w

68.7

3.8 4.0/40 4.5/30 7.6/20 7.1/9 6.4 7.0/15 6.6/18 5.7/23 10.0/32 9.9/40 UP

LAWN π-o-w

+15

+37 RICE DRIVE

VAROLT. 28' +28

+40

RICE DRIVE +57

67.6 +50 30' CCI

EASY UP 6.4/30 7.3/16 7.5 8.3/15 7.3/28 10.6/30 10.3/40 UP

π-o-w

CCI 18' +15

ODT 29' +17

67.3 66.5 65.8 66.3 65.6 66.9 64. 64.5

LEVEE 7.8/30 5.6/12 9.3/7 8.8 9.5/16 8.2/21 11.1/27 10.6/40 UP

		1270.73	10.22	1260.51
194				
195+00				
196+00				
BM.			10.22	1260.51 (1760.4)
TP	0.68	1258.59	12.82	1257.91
198+00				
TP.	0.09	1245.98	12.70	1245.89
TP.	5.30	1242.48	8.80	1237.18
TP.	11.65	1253.79	0.34	1242.14
208+00				
209+00				

N S

FENCE 12' → 194+13

195+51

67.0	66.6	64.9	63.6	64.1	63.9	63.	64.	62.8	64.1
3.7	4.1	5.8	7.1	6.6	6.8	7.7	6.7	7.9	6.6
40	30	12	9	5		16	20	24	40

YARD — 25' + 17 — R-O-W

718 — 29' CEN

25' 443

	63.9	59.8	60.	60.5	59.6	60.6	60.3		
LEVEL	6.8	10.9	10.7	10.2	11.1	10.1	10.4	EDGE PAVE	
	25	8	5		16	18	30	R-O-W	

	57.	56.2	53.	53.9	54.3	53.5	55.	54.6	54.
EASY UP	1.6	2.4	5.6	4.7	4.3	5.1	3.6	4.0	4.6
	80	16	9	2		13	21	30	40

	45.8	43.3	43.4	42.6	45.	44.5	44.7
DRIVE	8.0	10.5	10.4	11.2	8.8	9.3	9.1
	50	8		10	16	30	

63 22' 420

442 31'

470 31'

85 22'

	48.7	47.2	47.5	48.0	48.1	48.8	
LEVEL	6.1	4.6	6.3	5.8	5.7	5.0	LEVEL DRIVE
GARDEN	16	12	10		11	30	LAWN

1253.79

+ H.I. - F.L.

209+

210+00

T.P. 7.80 1258.63 2.96 1250.83

211+00

212+00

150

213-

213+00

- N S

715 29 EEI.

DRIVE +27 24' ⌀

+46 24 ⌀

⌀ 21' +65 B
T
U
S

+78 20' ⌀

53.1 52.2 51.5 48.9 49.6 50.2 49.2 51.7 50.4 51.2
0.7/40 1.6/30 2.3/19 4.9/12.5 4.2/11 3.6 4.6/9 2.1/15 3.4/23.5 T-O-W 2.6/40

⌀ 16.5 +01

+84 24 ⌀

+91 29' CEI

53.9 50.9 51.6 52.2 51.2 54.1 54.6 51.9 52.2
LEVEL 4.7/20 7.7/12.5 7.0/11 6.4 7.4/9 4.5/15 4.0/25 6.7/30 6.4/40 T-O-W UP

53.5 +16 24 ⌀
55. 54.1 53.3 54.4 54.3 53.9
LEVEL OUT 3.6/21 5.1/11 4.5 5.3/10 4.2/13 4.3/30 4.7/40 T-O-W UP

+00
W/MOT DRIVE
54.4 +24 54.7 53.9 54.9 54.4 53.9 53.2
HOUSE LEVEL 55.4 55.3 3.2/30 3.3/20 4.2/10 3.9 4.6/10 3.7/13 4.2/27 4.7/30 5.4/40 T-O-W

+65 CEI
56.4 53.9 53.5 53.9 53.2 54.6 54.5 51.7 51.6
LEVEL OUT 7.7/20 4.8/13 5.1/10 4.7 5.4/9 4.0/12 4.1/17 6.9/27 7.0/40 UP

1258.63

213	+	HI	−	EL
213+50				
214+00				
TP	7.00	1253.15	12.48	1246.15
214+50				
BM.			6.86	1246.29
	2.02	1248.31		
215+00				
T.P.	3.11	1239.35	12.07	1236.24
215+50				
216+00				
	4.57	1230.91	13.01	1226.34
217+00				
219+00				

CEI 567173

N 5

29' +12

31' +32

29' +48

56.2 51.2 51.5 50.8 51. 48.5 48.8 49.9
2.4 7.4 7.1 7.8 7.6 10.1 9.8 8.7
21 8 11 14 27 30 40 UP

LEVEL OUT

54.1 47.2 47.9 46.9 47.7 47. 47.3
4.5 11.4 10.7 11.7 10.9 11.6 11.3
25 10 10 13 24 30 40 UP

LEVEL OUT GARDEN

49.8 42.3 43.3 42.3 44.5 44.6 44.6
3.4 10.9 9.9 10.9 8.7 8.6 8.6
26 11 10 18 30 40 UP

SLOPES NE

26' +53

26' +73

43.3 43.3 39.7 37.9 38.4 37.6 41.4 41.7 41.7
5.0 5.0 8.6 10.4 9.9 10.7 6.9 6.6 6.6
30 27 15 11 8 15 30 40 UP

SLOPES TONE

28' +25

+37

DRIVE +55

36.3 35.4 34. 34. 33.1 32.9 32.2 37.9 38.9
3.1 4.0 5.4 5.4 6.3 6.5 2.2 1.5 .50
40 30 15 9 10 20 30 40 UP

23' +57

CEI 26' +72

37.4 32.9 32.7 28.3 29.2 29.8 28.8 32.2 35.1 35.2
7.0 6.6 4.7 11.1 10.7 9.6 10.6 6.2 4.3 4.2
36 30 26 13 11 5 18 30 40 UP

LEVEL

24.7 21.6 21.9 22.2 22.6 21.7 25.8 26.7
6.7 9.3 9.0 8.7 8.3 9.2 5.1 4.7
27 14 12.5 10 9 18 30 LEVEL OUT

EASY UP OATS

1217.4
13.5
18
LEVEL OATS

1220.1
10.8
20
LEVEL P.Lay

1230.91

	+	HI	−	Elev
TP	1.21	1219.59	12.53	1218.38
214+00				
B.M. WROUG SPK			5.32	1214.27 (1213.00)

CK. LEVELS ON #10 USING B.M. ON CEI #667173
@ # 214+50 1246.29

TP	0.77	1247.06	12.79	1234.27
	1.29	1235.56	12.72	1222.84
	0.63	1223.47	9.22	1214.25
	2.47	1216.72	3.69	1213.05

N 5

15.1 16.1 16.8 16.1
4.5/13 3.5/12 2.8 3.5/9

B.M. SPK S ROOT 22" ASH # 10 EAST OF FROST DRIVE
219+??

6-24-50 CULVERT OUTLET SEC. C #10 STA 179+25± ELV.

BM				1215.58
	3.32	1218.90		
0+0				℄ Rd
0+15±				
1+0				
2+0				
3+0				
4+0				
5+0				
BM	3.72	1219.30	3.72	1215.58

W E

NEB Mdwell ℄ Cont. pg. 69

4.18

1211.6
7.30
F.L

1211.7

Gradual Up 7.23 6.59 7.23 6.71 6.98 LEV. OUT
7 3 4 10

1211.1

Easy up 7.48 7.10 7.82 7.01 7.21 LEV OUT
10 3 4 10

1210.7

Family Lev thru Easy to N&N 7.29 7.44 8.16 7.22 7.60 LEV E&S
10 3 4 10

1210.6

U.P North Easy Lev West 7.74 7.68 8.30 7.49 7.76 LEV
10 5 4 10

1210.3

Easy up New 8.02 7.66 8.60 7.65 7.78 LEV
4 5 10

Spk SET N Root 20" Maple S.S. of Rd ± 177+07 using
1215.58 NEB N Mdwell at ±179+75

7-27-50 + N1 - Ell

Hubs set at 13' 5 of ℄

BELL ST. GRADE STAKES FOR BUTTON DITCH ELV's.

FROM EAST TO WEST

110+0			3.7	81.98 ✓
110+50			4.4	81.28 ✓
111+0			5.0	80.68 ✓
111+50			5.8	79.88 ✓
112+0			5.9	79.78 ✓
112+50			6.3	
113+0			5.6	
113+5			5.8	
T.	5.90	1185.68		
T.P. 114+0			8.16	1179.78
115+0				
116+0			7.05	80.89
T	0.91	1187.94		
BM.				1187.03

5 pt N.W. Root 28" Maple 7½ West of Buttin Ditch

104+0		12.4	77.17 ✓	
104+50		11.7	77.87 ✓	
105+0		10.7	78.87 ✓	
105+50		9.1	80.47 ✓	
106+0		7.4	82.17 ✓	8-8-50 8.0
106+50		4.8	84.77 ✓	5.4
107+0		3.7	85.87 ✓	4.3
107+50		3.9	85.67 ✓	4.5, HI = 90.17
T	4.54	1189.57 ✓		
T.P. 108+0		0.65	1185.03 ✓	
108+50	FRO DRIVE	1.68	84.00 ✓	6.17
109+0		1.9	83.78 ✓	
109+50		2.9	82.78 ✓	
	1185.68 ✓			

100+50		10.4		
101+0		11.2		
101+50		12.0		
102+0		12.7	76.87	
102+50		13.3	76.27	✓
103+0		12.9	76.67	✓
103+50		12.9	76.67	✓
	1189.57 ✓			

11/14/50 Nellie M. Coates (formly Jos. Morton) pg 53 Merritt & Zettimer 68

#1 Water well problem.

	+3.02	1190.05	1187.03
T.P.	-3.98		1186.07
	+6.45	1192.52	
T.P.	-8.00		1184.52
	+11.84	1196.36	
	-0.74		1195.62
	-20.24		1176.12 Top H2O
	-22.24		1174.12 Bottom Well
	6.87		89.52
	10.14		86.22
New Set	+1.36	1185.88	1184.52
	-14.55		1171.33
	-13.10		1172.78
	-11.10		74.78 Top H2O
	12.10		73.78 Bot "

BM #6 = Bent spk = N.W. root (most Westly maple)
= 7th Maple W. of Button drive = 25' S. of 118+75

Stone 5 E & Mitchell barn (Coates)

Stone ±100 ft N. of W. end house

Stone porch floor rear Mitchell (Coates) house

Rear Coates House (Well)
Suction pipe in well
Old H2O level in "

Bot creek ± old dam.

Inlet F.L. culvert under Cemetery drive

24" tile ±35' S th of creek at old dam

See pg 51 & 53
± Feb. 1950

5-22-57 Culvert Bell St
Sta. 179±25 (SEE Pg 64)

BM 4.46 1220.04 1215.58
Set ± ℄ #10 west of culvt
15 from ± ℄ east

Stadia	Ang Rt Rod			
		9.65	1210.35	OUTLET H_2O 1E INLET
		9.27	1210.73	H_2O 1E
100	102-13	7.5	1212.5	MEADOW
100	88-45	7.8	1212.2	W. BANK
100	86-45	8.3	1211.7	CH'l H_2O 0E
100	82-15	6.85	1213.1	E. Bank
100	80-33	7.7	1212.3	Edge wheat
112	68-20	7.5	1212.5	Lev 15' thereon
200	82-50	7.4	1212.6	wheat
200	92-42	7.8	1212.2	Edge Wh't
200	94-00	7.1	1212.9	E BANK

200	96-00	8.7	1211.3	Ch'l H_2O 0E
200	97.35	7.1	1212.9	W Bank
200	103-00	7.7	1212.3	Meadow
300	105-50	7.8	1212.2	"
300	100-10	7.5	1212.5	W Bank
300	98-57	9.0	1211.0	H_2O 0E Chan'l
300	97.40	7.3	1212.7	E. Bank
300	97-00	7.9	1212.1	Edge Wh't
300	90-48	7.8	1212.2	Wh't
370	90-00	8.1	1211.9	0E H_2O in wheat
370	98-15	8.6	1211.4	0E H_2O W'l in Wh't
370	98-08	7.6	1212.4	E bank
370	100-07	9.0	1211.0	H_2O 1E Chan'l

OPENING IN 370

CONT ON SHEET MARKED 69A

20+09

20"x22"x20.5' Stone culvt
edwy 16' Poor cond. Replace

14+37.04 ○ ~~Spk set~~ POT

BELL ST.

9+34.76 ○ Spk sunk
65.24

1+64 9½" C.I.P. x 24' culvt
Replace with 12" & lengthen

All stks set at 25°

0+02.75 Δ: 79-28
I.P. set

460.95
151-09-30
150-32
657.69
93-24
460.95 to P.I.
25°

11.1

S&W in NE root 24" Elm

48.18

(Mon. Box Set 1963) (1) 20.43 S&W in W side 15" Maple

37.38

S&W in SE root 50" Elm

25° I.P. Fd

det 89-13

937

Stone Mon. 33.36

12.5

24'

20' Edwy

120.05

Newbury

So. Russell

FR 2 8.6

1" I.P. set = P.I.

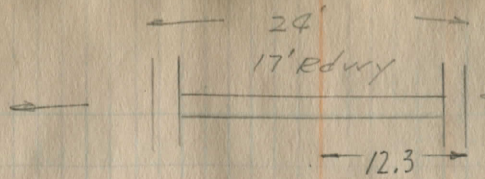
2.75

I.P. Fd 0.96

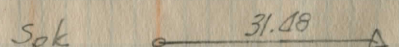
20.05

S&W N side 8" Elm

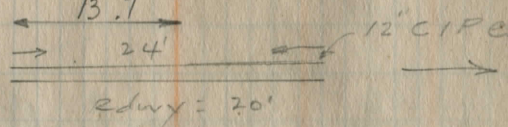
64+19 30" x 18" Stone culvt N.G. Replace



49+02.12

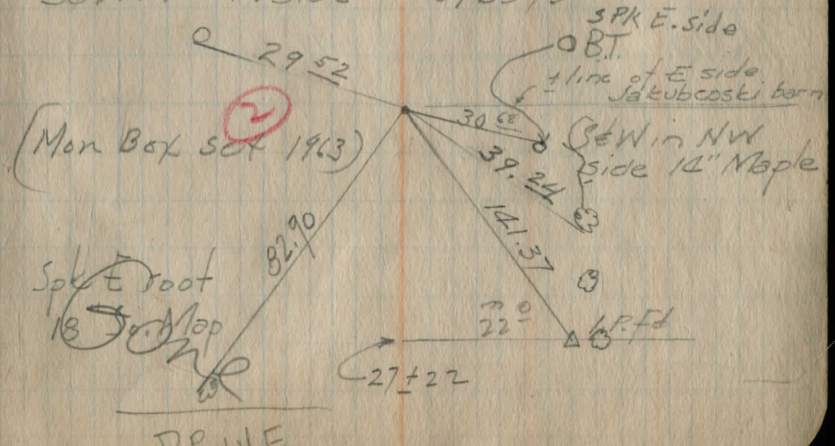


38+70 10" C.I.P. culvt Replace



28+61.38 ~~Spk set~~ 179-38 359-16

SdW in NW side ± 576573



J3.13

95+56.87 I.P. Fd 179-08-30

walls
Rotten conc. & undermined

85+85 30"x 18"x 3.5 Conc. culvt
N.G. Replace

72+25 10"x 20' C.I.P.
Pipe OK

89.41
179-22

69+69.26 179-53-30

30°

I.P. Fd

spk NW side
CEI 194827

61.70

31.33 I.P. P/L

92.33

I.P. P/L N of CEI

E 194826 old P/W

23.5

91.50 18' Rdwy

spk SW side CEI.

Pond

11.8

18'

12" VSP

20' Rdwy

24'

13.9

spk side Tel. pole
Replace if for route paid

(Mon Box set 1963)

10" CIP

℄ Main

~~Reset 63 spk Fd~~

124.20 Spk W side 24" Map

31.35

43.30

Hub

Spk NW side CEI

106.78

Spk N side 20" Map

112+13 24" x ±18" x 26' Stone culvt
Very poor drainage above & below

179.09
359.38

108+62.5 Bolt set

102+21.5 2-15" x 32.5' Conc pipe culvt

I.P. P/L △ 26.25 116+35.2

swamp

26'
24' Rdwy

12.8

dir. of flow

±24" VSP

Button

27.5 I.P. P/L Frehring

57.97

44.80

Spk. NE side CEI # 585790

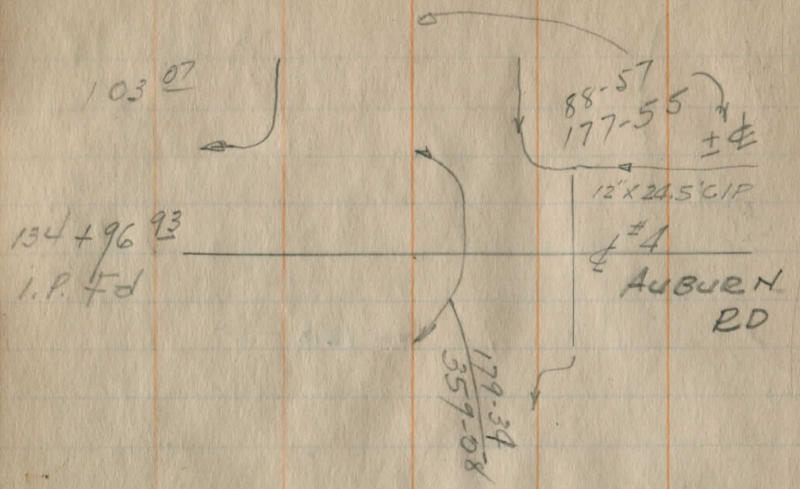
Spk. NW side 6" W. Ch

rdwy can be increased N without adding pipe

20' rdwy
32.5'

pond

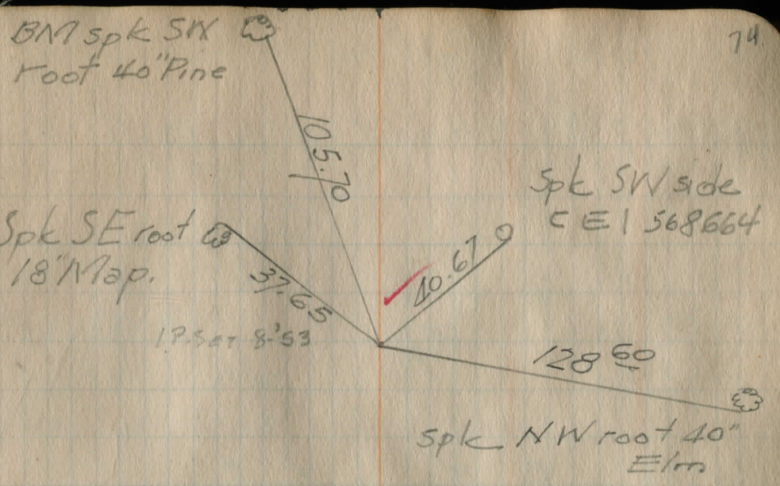
15.3

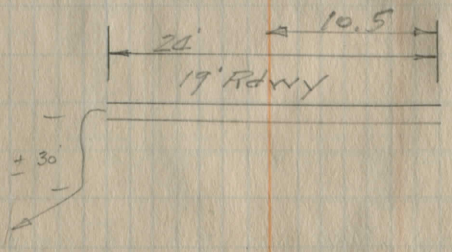


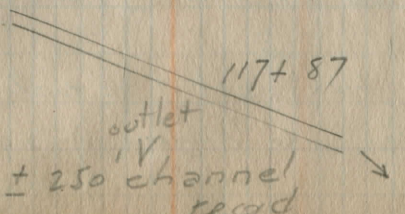
122+69

10"x24'C.I.P.
pipe OK

No outlet exist.
Place 15" R.C.P. on NE-SW
skew







102 80

179.31
359.02

158+97.20 T. Hub Fd

9' both Bs

spk E root 18" Maple

29.64

67.67

48 32

Spk SE side CE 1 #567202

Spk SW root 48" So. Map Front of Knox

156+82 B 9' 7' B

25.0
24.75

156+81.5 1.P.Fd

154 B 13' 6' B

Hders ± 1' high

9.1 9.9

18.0

20' slab

17.8' clear span

149+23.3

8.73 9.24

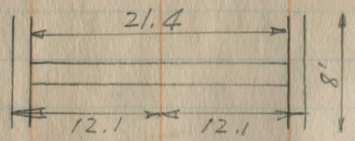
Spk SET on ℄ 0.10 W of SLAB

New Conc. slab on ± 8" I beams
Stone abut
Slab extends ± 1.0 beyond abuts

Note Max. pavt ± 30' each side of
bridge = 16' because of narrow approach

184	B	9.5	10	B
182	B	7.5	12'	B

179+25



Conc box culv. exc. cond
3' span. Has Floor ± 10" mud over Floor
Ht opening = 2'

192+97.25

178	B	10.5	10	B
174	B	11'	7.5	B

171+97.25 P.O.T.

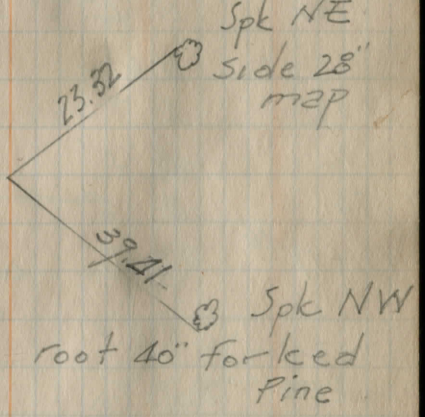
167+56 ± 6" field tile. Place larger pipe on ± 45° skew SE

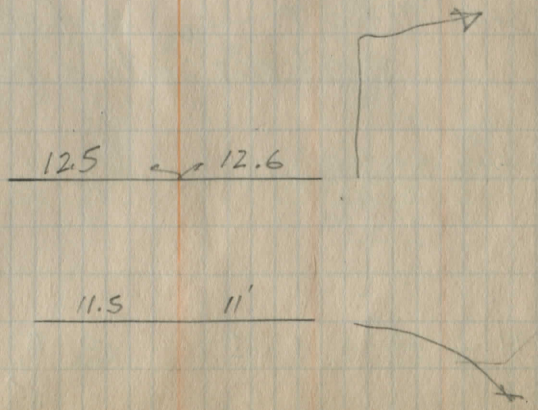
167+80 ± 9" C.I.P.
Place larger pipe & open up 50' of outlet

Z

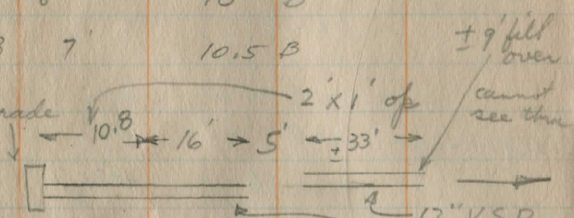
R.R. Spk set

Reset 0.11' South & reref — Done





210	B	10'	9'	B	
206	B	8'	10'	B	
204	B	7'	10.5	B	



203+78					
202	B	6'	12'	B	
200	B	6'	10'	B	
198	B	7'	13	B	
196	B	5'	15'	B	
194	B	6'	15'	B	

192+97 ±48 P.O.T. Δ I.P.Fd (Bent, use .35 S of head)
0.30 S

192+40	B	7'	12'	B	

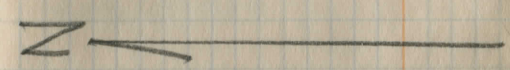
192+40 P.O.T. Bent spk set
Reset 0.29 South & reref Done

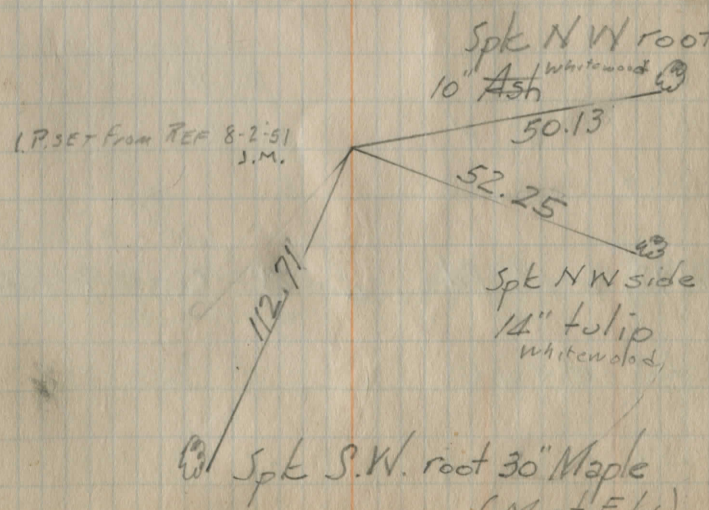
191	B	8.5	12'	B	

185 ±30 30.35 Δ I.P.Id

Old Stone culvert Replace

Note: Side stks 158+97 To 212+00 slightly off line





230	B	13	7' B
228	B	13	5' B

Note Stks 214 - 224 0.0 to 0.4' off line (S)

226	B	12.5	5.5 B
224	B	12'	6' B
222	B	12	6' B
220	B	11	6' "

219+10 Spk Set POT

216	B	11'	8' B
214	B	9'	8.5 B

101.81

212+98.19 I.P. Fd △ Δ = 0-09 Rt

our line 0.47 N of I.P.

212+80	B	9'	7.5 B

298 3°

N

B.M. spk 20" Ash

25.11 — Final align. = ±0.20 North

Drive

57.20

Reset & ref done

Spk SW side 20 Ash

Spk S side 24" map

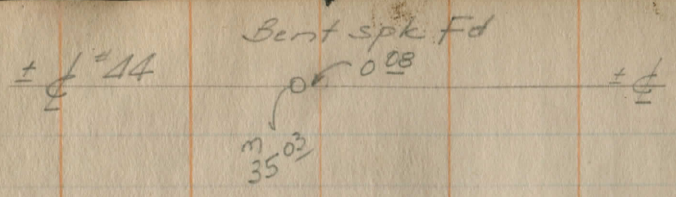
57.91

Spk NW side 15" Map

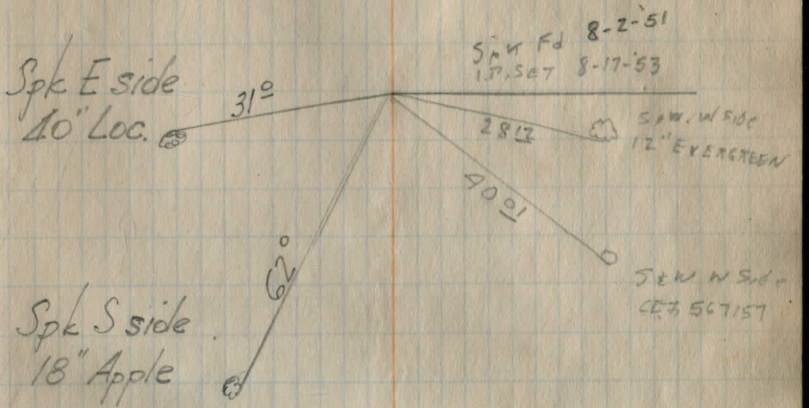
32.79

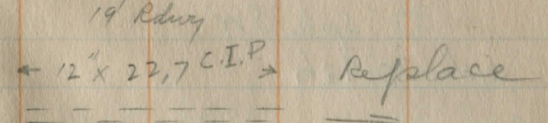
29.85 — I.P. Fd

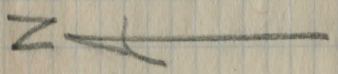
I.P. Set from Refs 9-7-51 J.M.



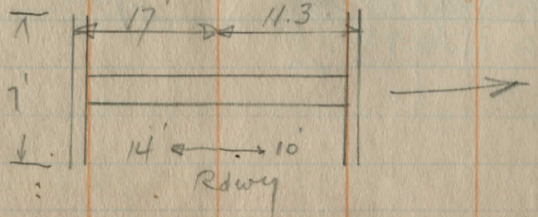
242+81.7 P.O.T







238	B	10'	9'	B
236	B	10'	9'	B
234	B	12'	8'	B



3'x1' opening fullas of 3/27/50

Conc. Culvt ok

clean deepen ± 100' outlet

7-27-50 BEN S7

HUBS SET 13' S of ℄ EVERY 50', 100+50 to 114+0. Also 115+0 & 116+0

IMPROVED TABLES

AND

INFORMATION

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope 1½ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

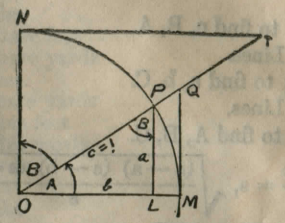


TABLE II

TRIGONOMETRIC FORMULÆ.

$\angle A = \angle MOP \qquad \angle B = \angle PON = \angle OPL$

$R = OB = c = 1$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \tfrac{1}{2} A = \sqrt{\frac{1 - \text{Cos } A}{2}} \qquad \cos \tfrac{1}{2} A = \sqrt{\frac{1 + \text{Cos } A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \qquad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Lines} \quad \frac{\sin A}{a} = \frac{\sin B}{B} = \frac{\sin C^1}{C}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \tfrac{1}{2}(A+B)}{\tan \tfrac{1}{2}(A-B)}$$

TABLE II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find **c, B, A.**

Use Law of Lines.

Given A, B, c; to find **a, b, C.**

Use Law of Lines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)\ (s-b)\ (s-c)}{s}} = r$$

$$\cos \tfrac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \tfrac{1}{2} A = \frac{r}{s-a}$$

$$\tan \tfrac{1}{2} B = \frac{r}{s-b}$$

$$\tan \tfrac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \tfrac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s\ (s-a)\ (s-b)\ (s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6}(B+b+4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11	
1/16	.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219	1/16
1/8	.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271	1/8
3/16	.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323	3/16
1/4	.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375	1/4
5/16	.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	6927	.7760	.8594	.9427	5/16
3/8	.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479	3/8
7/16	.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531	7/16
1/2	.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583	1/2
9/16	.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635	9/16
5/8	.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688	5/8
11/16	.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740	11/16
3/4	.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792	3/4
13/16	.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844	13/16
7/8	.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896	7/8
15/16	.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948	15/16
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.000	1
	0	1	2	3	4	5	6	7	8	9	10	11	

TABLE IV
USEFUL RELATIONS.

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links

360° = 21600′ = 1296000″

Radius = arc of 57.2957790°

Arc of 1° (radius = 1) = .017453292

Arc of 1′ (radius = 1) = .000290888

Arc of 1″ (radius = 1) = .000004848

$\pi = 3.141592654$

$\sqrt{\frac{1}{4}} = 0.564190$

$\frac{\pi}{4} = 0.785398163$

$\sqrt[3]{\frac{6}{\pi}} = 1.240700982$

$\frac{\pi}{6} = 0.523598776$

$\pi^2 = 9.869604401$

$\sqrt{\frac{4}{\pi}} = 1.128379167$

$\frac{1}{\pi^2} = 0.101321184$

$\frac{\pi}{6} = 0.523598776$

$\sqrt{\pi} = 1.772453851$

$\frac{4.\pi}{3} = 4.188790205$

$\frac{1}{\pi} = 0.3183099$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)²

Difference between arc and chord length, 0.05 feet in 11½ miles

Probable error of a single observation $= 0.6754\sqrt{\frac{\Sigma v^2}{n-1}}$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULÆ.

Horizontal Distance = $R - R \sin^2 a + C \cos a$

Vertical Distance = $R \tfrac{1}{2} \sin 2a + C \sin a$

$R = \text{Reading} \times \frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

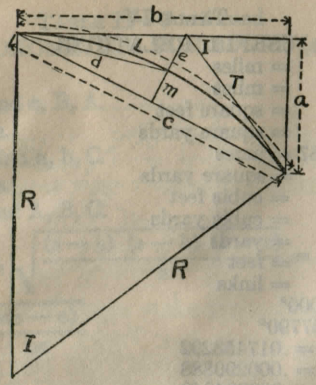


Table V

CURVE FORMULAE FOR SIMPLE CURVES

Compiled by J. Calvin Locke, C.E.

(1) $c = \sqrt{2Ra}$ (2) $c = \sqrt{a^2+b^2}$

(3) $c = \sqrt{2R\,(R-\sqrt{(R+b)\,(R-b)}} = \sqrt{2R(R-\sqrt{R^2-b^2})}$

(4) $c = 2\sqrt{m\,(2R-m)}$

(5) $c = 2R \sin \frac{1}{2} I$ (6) $c = 2T \cos \frac{1}{2} I$

(7) $e = R \operatorname{exsec} \frac{1}{2} I$

(8) $e = R \tan \frac{1}{2} I \tan \frac{1}{4} I$ (9) $e = T \tan \frac{1}{4} I$

(10) $b = \sqrt{a\,(2R-a)}$

(11) $b = \sqrt{\left(c+\frac{c^2}{2R}\right)\left(c-\frac{c^2}{2R}\right)} = \sqrt{c^2-\frac{c^4}{4R^2}}$

(12) $b = R \sin I$ (13) $b = a \cot \frac{1}{2} I$

(14) $R = \frac{a^2+b^2}{2a} = \frac{c^2}{2a}$ (15) $R = \frac{d^2}{2m} = \frac{c^2+4m^2}{8m}$

(16) $d = \sqrt{R\,(2R-\sqrt{(2R+c)\,(2R-c)}} = \sqrt{R(2R-\sqrt{4R^2-c^2})}$

(17) $d = \sqrt{2Rm}$ (18) $d = 2R \sin \frac{1}{4} I$ (19) $m = \frac{d^2}{2R}$

(20) $m = R \mp \sqrt{\left(R+\frac{c}{2}\right)\left(R-\frac{c}{2}\right)} = R \mp \sqrt{R^2-\frac{c^2}{4}}$

(21) $m = R \operatorname{vers} \frac{1}{2} I$ (22) $m = R \sin \frac{1}{2} I \tan \frac{1}{4} I$ (23) $m = \frac{1}{2} c \tan \frac{1}{4} I$

(24) $a = \frac{c^2}{2R}$ (25) $a = R - \sqrt{(R+b)\,(R-b)} = R - \sqrt{R^2-b^2}$

(26) $a = 2R\,(\sin^2 \frac{1}{2} I)^2$ (27) $a = R \operatorname{vers} I$ (28) $a = R \sin I \tan \frac{1}{2}$

(29) $a = b \tan \frac{1}{2} I$ (30) $a = T \sin I$ (31) $T = R \tan \frac{1}{2} I$

(32) $I = \frac{L}{R} \times 57.295780$ (33) $R = \frac{L}{I} \times 57.295780$

(34) $L = IR \times 0.01745329$ (35) $L = \frac{8d-c}{3}$

(36) Area Seg. $= \frac{LR - R^2 \sin I}{2} = \frac{LR - Rb}{2}$

Table VI

SINES, COSINES, TANGENTS, COTANGENTS

deg.	sin 0′	tan 0′	sin 10′	tan 10′	sin 20′	tan 20′	sin 30′	tan 30′	sin 40′	tan 40′	sin 50′	tan 50′	deg.
0	0000	0000	0029	0029	0058	0058	0087	0087	0116	0116	0145	0145	89
1	175	0375	0204	0204	0233	0233	0262	262	291	291	320	320	88
2	349	349	378	378	407	407	436	437	465	466	494	495	87
3	523	524	552	553	581	582	610	612	640	641	669	706	86
4	698	699	727	729	756	758	785	787	814	816	843	864	85
5	872	875	901	904	929	934	958	963	987	992	1016	1022	84
6	1045	1051	1074	1080	1103	1110	1132	1139	1161	1169	190	198	83
7	219	228	248	257	279	287	305	317	334	346	363	376	82
8	392	405	421	435	449	465	478	495	507	524	536	554	81
9	564	584	593	614	622	644	650	673	679	703	708	733	80
10	736	763	765	793	794	823	822	853	851	883	880	914	79
11	908	944	937	974	965	2004	994	2035	2022	2065	2051	2095	78
12	2079	2126	2108	2156	2136	186	2164	217	193	247	221	278	77
13	250	309	278	339	306	370	334	401	363	432	391	462	76
14	419	493	447	524	476	555	504	586	532	617	560	648	75
15	588	679	616	711	644	742	672	773	700	805	728	836	74
16	756	867	784	899	812	931	840	962	868	994	896	3026	73
17	924	3057	952	3089	939	3121	3007	3153	3035	3185	3062	217	72
18	3090	249	3118	281	3145	314	173	346	201	378	228	411	71
19	256	443	283	476	311	508	338	541	365	574	393	607	70
20	420	640	448	673	475	706	502	739	529	772	557	805	69
21	584	839	611	872	638	906	665	939	692	973	719	4006	68
22	746	4040	773	4074	800	4108	827	4142	854	4176	881	210	67
23	907	245	934	279	961	314	987	348	4014	383	4041	417	66
24	4067	452	4094	487	4120	522	4147	557	173	592	200	628	65
25	226	663	253	699	279	734	305	770	331	806	358	841	64
26	384	877	410	913	436	950	4462	986	488	5022	514	5059	63
27	540	5095	566	5132	592	5169	617	5206	643	243	669	280	62
28	695	317	720	354	746	392	772	430	797	467	823	505	61
29	848	543	874	581	899	619	924	658	950	696	975	735	60
30	5000	774	5025	5812	5050	851	5075	890	5100	930	5125	969	59
31	150	6009	175	6048	200	6088	225	6128	250	6168	275	6208	58
32	299	249	324	289	348	330	5373	371	398	412	422	453	57
33	446	494	471	536	495	577	519	619	544	661	568	703	56
34	592	745	616	787	640	830	664	873	688	916	712	959	55
35	736	7002	760	7046	783	7089	807	7133	831	7177	854	7221	54
36	878	265	901	310	925	355	948	400	972	445	995	490	53
37	6018	536	6041	581	6065	627	6088	673	6111	720	6134	766	52
38	157	813	180	860	202	907	225	954	248	8002	271	8050	51
39	293	8098	316	8146	338	8195	361	8243	383	292	406	342	50
40	428	391	450	441	472	491	494	541	517	591	539	642	49
41	561	693	583	744	604	796	626	847	648	899	670	952	48
42	691	9004	713	9057	734	9110	756	9163	777	9217	799	9271	47
43	820	325	841	380	862	435	884	490	905	545	926	601	46
44	947	657	967	713	988	770	7009	827	7030	884	7050	942	45
45	7071	1.0000	7092	1.0058	7112	1.0117	133	1.0176	153	1.0235	173	1.0295	44
deg.	60′ cos	60′ cot	50′ cos	50′ cot	40′ cos	40′ cot	30′ cos	30′ cot	20′ cos	20 cot	10′ cos	10′ cot	deg.

TABLE VI (continued)

SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg.	sin 0′	tan 0′	sin 10′	tan 10′	sin 20′	tan 20′	sin 30′	tan 30′	sin 40′	tan 40′	sin 50′	tan 50′	deg.
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	.2349	790	.2423	808	.2497	826	.2572	844	.2647	862	.2723	38
52	880	.2799	898	.2876	916	.2954	934	.3032	951	.3111	969	.3190	37
53	986	.3270	8004	.3351	8021	.3452	8039	.3514	8056	.3597	8073	.3680	36
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4106	175	.4193	35
55	192	.4281	208	.4370	225	.4460	241	.4550	258	.4641	274	.4733	34
56	290	.4826	307	.4919	323	.5013	339	.5108	355	.5204	371	.5301	33
57	387	.5399	403	.5497	418	.5597	434	.5697	450	.5798	465	.5900	32
58	480	.6003	496	.6107	511	.6212	526	.6319	542	.6426	557	.6534	31
59	572	.6643	587	.6753	601	.6864	616	.6977	631	.7090	646	.7205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2 0655	9013	2 .0809	9026	.0965	9038	.1123	9051	.1283	25
65	9063	.1445	075	.1609	088	.1775	100	.1943	112	.2113	124	.2286	24
66	135	.2460	147	.2637	159	.2817	171	.2998	182	3183	194	.3369	23
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20
70	397	2.7475	9407	2.7725	9417	2. 7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16
74	613	.4874	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	11
79	816	.1446	822	5.2257	827	5. 3093	833	5.3955	838	5.4845	843	.5764	10
80	9848	5.6713	9853	5.7694	9858	5. 8708	9863	5.9758	9868	6.0844	9872	6.1970	9
81	877	6.3138	881	6.4348	886	6. 5606	890	6.6912	894	.8269	899	.9682	8
82	903	7.1154	907	7.2687	911	7. 4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8. 5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	9995	31.242	9996	34.368	997	38.189	997	42.964	9998	49.104	1
89	9998	57.290	9999	68.750	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	0
deg.	60′ cos	60′ cot	50′ cos	50′ cot	40′ cos	40′ cot	30′ cos	30′ cot	20′ cos	30′ cot	10′ cos	10′ cot	deg.

TABLE VII

RODS IN FEET AND INCHES

Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches
1	16—6	21	346—6	41	676—6	61	1006—6	81	1336—6
2	33—0	22	363—0	42	693—0	62	1023—0	82	1353—0
3	49—6	23	379—6	43	709—6	63	1039—6	83	1369—6
4	66—0	24	396—0	44	726—0	64	1056—0	84	1386—0
5	82—6	25	412—6	45	742—6	65	1072—6	85	1402—6
6	99—0	26	429—0	46	759—0	66	1089—0	86	1419—0
7	115—6	27	445—6	47	775—6	67	1105—6	87	1435—6
8	132—0	28	462—0	48	792—0	68	1122—0	88	1452—0
9	148—6	29	478—6	49	808—6	69	1138—6	89	1468—6
10	165—0	30	495—0	50	825—0	70	1155—0	90	1485—0
11	181—6	31	511—6	51	841—6	71	1171—6	91	1501—6
12	198—0	32	528—0	52	858—0	72	1188—0	92	1518—0
13	214—6	33	544—6	53	874—6	73	1204—6	93	1534—6
14	231—0	34	561—0	54	891—0	74	1221—0	94	1551—0
15	247—6	35	577—6	55	907—6	75	1237—6	95	1567—6
16	264—0	36	594—0	56	924—0	76	1254—0	96	1584—0
17	280—6	37	610—6	57	940—6	77	1270—6	97	1600—6
18	297—0	38	627—0	58	957—0	78	1287—0	98	1617—0
19	313—6	39	643—6	59	973—6	79	1303—6	99	1633—6
20	330—0	40	660—0	60	990—0	80	1320—0	100	1650—0

TABLE VIII

LINKS IN FEET AND INCHES

Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches
1	0- 7.92	18	11-10.56	35	23- 1.20	52	34- 3 84	69	45- 6 48	86	56- 9 12
2	1- 3.84	19	12- 6.48	36	23- 9.12	53	34-11 76	70	46- 2 40	87	57- 5 04
3	1-11.76	20	13- 2.40	37	24- 5.04	54	35- 7 68	71	46-10 32	88	58- 0 96
4	2- 7.68	21	13-10.32	38	25- 0.96	55	36- 3 60	72	47- 6.24	89	58- 8.88
5	3- 3.60	22	14- 6.24	39	25- 8.88	56	36-11 52	73	48- 2 16	90	59- 4 80
6	3-11.52	23	15- 2.16	40	26- 4.80	57	37- 7.44	74	48-10 08	91	60- 0 72
7	4- 7.44	24	15-10.08	41	27- 0.72	58	38- 3 36	75	49- 6 00	92	60- 8 64
8	5- 3.36	25	16- 6.00	42	27- 8.64	59	38-11 28	76	50- 1 92	93	61- 4 56
9	5-11.28	26	17- 1.92	43	28- 4.56	60	39- 7 20	77	50- 9.84	94	62- 0 48
10	6- 7.20	27	17- 9.84	44	29- 0.48	61	40- 3 12	78	51- 5 76	95	62- 8 40
11	7- 3.12	28	18- 5.76	45	29- 8.40	62	40-11 04	79	52- 1.68	96	63- 4 32
12	7-11.04	29	19- 1.68	46	30- 4.32	63	41- 6.96	80	52- 9 60	97	64- 0 24
13	8- 6.96	30	19- 9.60	47	31- 0.24	64	42- 2.88	81	53- 5.52	98	64- 8 16
14	9- 2.88	31	20- 5.52	48	31- 8.16	65	42-10.80	82	54- 1 44	99	65- 4 08
15	9-10.80	32	21- 1 44	49	32- 4.08	66	43- 6.72	83	54- 9 36	100	66- .000
16	10- 6.72	33	21- 9.36	50	33- 0.00	67	44- 2 64	84	55- 5.28	101	66 -7 92
17	11- 2.64	34	22- 5.28	51	33- 7.92	68	44-10.56	85	56- 1.20	102	67- 3.84

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=10°	I	T	E	I=20°	I	T	E	I=30'
1°	50.00	.218	+	11°	551.70	26.500	+	21°	1061.9	97.577	+
10′	58.34	.297	5° C.	10′	560.11	27.313	5° C	10′	1070.6	99.155	5° C
20′	66.67	.388	T	20′	568.53	28.137	T	20′	1079.2	100.75	T
30′	75.01	.491	.03	30′	576.95	28.974	.06	30′	1087.8	102.35	.10
40′	83.34	.606	E	40′	585.36	29.824	E	40′	1096.4	103.97	E
50′	91.68	.733		50′	593.79	30.686		50′	1105.1	105.60	
2°	100.01	.873	.001	12°	602.21	31.561	.006	22°	1113.7	107.24	.013
10′	108.35	1.024		10′	610.64	32.447		10′	1122.4	108.90	
20′	116.68	1.188		20′	619.07	33.347		20′	1131.0	110.57	
30′	125.02	1.364		30′	627.50	34.259		30′	1139.7	112.25	
40′	133.36	1.552		40′	635.93	35.183		40′	1148.4	113.95	
50′	141.70	1.752		50′	644.37	36.120		50′	1157.0	115.66	
3°	150.04	1.964	10° C.	13°	652.81	37.070	10° C.	23°	1165.7	117.38	10° C.
10′	158.38	2.188	T	10′	661.25	38.031	T	10′	1174.4	119.12	T
20′	166.72	2.425	.06	20′	669.70	39.006	.13	20′	1183.1	120.87	.19
30′	175.06	2.674	E	30′	678.15	39.993	E	30′	1191.8	122.63	E
40′	183.40	2.934	.003	40′	686.60	40.992	.011	40′	1200.5	124.41	.025
50′	191.74	3.207		50′	695.06	42.004		50′	1209.2	126.20	
4°	200.08	3.492		14°	703.51	43.029		24°	1217.9	128.00	
10′	208.43	3.790		10′	711.97	44.066		10′	1226.6	129.82	
20′	216.77	4.099		20′	720.44	45.116		20′	1235.3	131.65	
30′	225.12	4.421		30′	728.90	46.178		30′	1244.0	133.50	
40′	233.47	4.755		40′	737.37	47.253		40′	1252.8	135.35	
50′	241.81	5.100	15° C.	50′	745.85	48.341	15° C.	50′	1261.5	137.23	15° C.
5°	250.16	5.459	T	15°	754.32	49.441	T	25°	1270.2	139.11	T
10′	258.51	5.829	.09	10′	762.80	50.554	.19	10′	1279.0	141.01	.29
20′	266.86	6.211	E	20′	771.29	51.679	E	20′	1287.7	142.93	E
30′	275.21	6.606	.004	30′	779.77	52.818	.017	30′	1296.5	144.85	.038
40′	283.57	7.013		40′	788.26	53.969		40′	1305.3	146.79	
50′	291.92	7.432		50′	796.75	55.132		50′	1314.0	148.75	
6°	300.28	7.863		16°	805.25	56.309		26°	1322.8	150.71	
10′	308.64	8.307		10′	813.75	57.498		10′	1331.6	152.69	
20′	316.99	8.762		20′	822.25	58.699		20′	1340.4	154.69	
30′	325.35	9.230		30′	830.76	59.914		30′	1349.2	156.70	
40′	333.71	9.710	20° C.	40′	839.27	61.141	20° C.	40′	1358.0	158.72	20° C.
50′	342.08	10.202	T	50′	847.78	62.381	T	50′	1366.8	160.76	T
			.13				.26				.39
7°	350.44	10.707	E	17°	856.30	63.634	E	27°	1375.6	162.81	E
10′	358.81	11.224	.006	10′	864.82	64.900	.022	10′	1384.4	164.86	.051
20′	367.17	11.753		20′	873.35	66.178		20′	1393.2	166.95	
30′	375.54	12.294		30′	881.88	67.470		30′	1402.0	169.04	
40′	383 91	12.847		40′	890.41	68.774		40′	1410.9	171.15	
50′	392.28	13.413		50′	898.95	70.091		50′	1419.7	173.27	
8°	400.66	13.991		18°	907.49	71.421		28°	1428.6	175.41	
10′	409.03	14.582		10′	916.03	72.764		10′	1437.4	177.55	
20′	417.41	15.184	25° C.	20′	924.58	74.119	25° C.	20′	1446.3	179.72	25° C.
30′	425.79	15.799	T	30′	933.13	75.488	T	30′	1455.1	181.89	T
40′	434.17	16.426	.16	40′	941.69	76.869	.32	40′	1464.0	184.08	.49
50′	442.55	17.065	E	50′	950.25	78.264	E	50′	1472.9	186.29	E
9°	450.93	17.717	.007	19°	958.81	79.671	.028	29°	1481.8	188.51	.065
10′	459.32	18.381		10′	967.38	81.092		10′	1490.7	190.74	
20′	467.71	19.058		20′	975.96	82.525		20′	1499.6	192.99	
30′	476.10	19.746		30′	984.53	83.972		30′	1508.5	195.25	
40′	484.49	20.447		40′	993.12	85.431		40′	1517.4	197.53	
50′	492.88	21.161		50′	1001.7	86.904		50′	1526.3	199.82	
10°	501.28	21.887	30° C.	20°	1010.3	88.389	30° C.	30°	1535.3	202.12	30° C.
10′	509.68	22.624	T	10′	1018.9	89.888	T	10′	1544.2	204.44	T
20′	518.08	23.375	.19	20′	1027.5	91.399	.39	20′	1553.1	206.77	.59
30′	526.48	24.138	E	30′	1036.1	92.924	E	30′	1562.1	209.12	E
40′	534.89	24.913	.008	40′	1044.7	94.462	.034	40′	1571.0	211.48	.078
50′	543.29	25.700		50′	1053.3	96.013		50′	1580.0	213.86	

T = R tan ½ I E = R exsec ½ I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=40°	I	T	E	I=50°	I	T	E	I=60°
31°	1589.0	216.3	+	41°	2142.2	387.4	+	51°	2732.9	618.4	+
10′	1598.0	218.7	5° C.	10′	2151.7	390.7	5° C.	10′	2743.1	622.8	5° C.
20′	1606.9	221.1	T	20′	2161.2	394.1	T	20′	2753.4	627.2	T
30′	1615.9	223.5	.13	30′	2170.8	397.4	.17	30′	2763.7	631.7	.21
40′	1624.9	226.0	E	40′	2180.3	400.8	E	40′	2773.9	636.2	E
50′	1633.9	228.4		50′	2189.9	404.2		50′	2784.2	340.7	
32°	1643.0	230.9	.023	42°	2199.4	407.6	.037	52°	2794.5	645.2	.056
10′	1652.0	233.4		10′	2209.0	411.1		10′	2804.9	649.7	
20	1661.0	235.9		20′	2218.6	414.5		20′	2815.2	654.3	
30′	1670.0	238.4		30′	2228.1	418.0		30′	2825.6	658.8	
40′	1679.1	241.0		40′	2237.7	421.4		40′	2835.9	663.4	
50′	1688.1	243.5		50′	2247.3	425.0		50′	2846.3	668.0	
33°	1697.2	246.1	10° C.	43°	2257.0	428.5	10° C.	53°	2856.7	672.7	10° C.
10′	1706.3	248.7	T	10′	2266.6	432.0	T	10′	2867.1	677.3	T
20′	1715.3	251.3	.26	20′	2276.2	435.6	.34	20′	2877.5	682.0	.42
30′	1724.4	253.9	E	30′	2285.9	439.2	E	30′	2888.0	686.7	E
40′	1733.5	256.5	.046	40′	2295.6	442.8	.075	40′	2898.4	691.4	.112
50′	1742.6	259.1		50	2305.2	446.4		50′	2908.9	696.1	
34°	1751.7	261.8		44°	2314.9	450.0		54°	2919.4	700.9	
10′	1760.8	264.5		10′	2324.6	453.6		10′	2929.9	705.7	
20′	1770.0	267.2		20′	2334.3	457.3		20′	2940.4	710.5	
30′	1779.1	269.9		30′	2344.1	461.0		30′	2951.0	715.3	
40′	1788.2	272.6		40′	2353.8	464.6		40′	2961.5	720.1	
50′	1797.4	275.3	15° C.	50′	2363.5	468.4	15° C.	50′	2972.1	725.0	15° C.
35°	1806.6	278.1	T	45°	2373.3	472.1	T	55°	2982.7	729.9	T
10′	1815.7	280.8	.40	10′	2383.1	475.8	.51	10′	2993.3	734.8	.63
20′	1824.9	283.6	E	20′	2392.8	479.6	E	20′	3003.9	739.7	E
30′	1834.1	286.4	.070	30′	2402.6	483.4	.116	30′	3014.5	744.6	.168
40′	1843.3	289.2		40′	2412.4	487.2		40′	3025.2	749.6	
50′	1852.5	292.0		50′	2422.3	491.0		50′	3035.8	754.6	
36°	1861.7	294.9		46°	2432.1	494.8		56°	3046.5	759.6	
10′	1870.9	297.7		10′	2441.9	498.7		10′	3057.2	764.6	
20′	1880.1	300.6		20′	2451.8	502.5		20′	3067.9	769.7	
30′	1889.4	303.5		30′	2461.7	506.4		30′	3078.7	774.7	
40′	1898.6	306.4	20° C.	40′	2471.5	510.3	20° C.	40′	3089.4	779.8	20° C.
50′	1907.9	309.3	T	50′	2481.4	514.3	T	50′	3100.2	784.9	T
			.53				.68				.84
37°	1917.1	312.2	E	47°	2491.3	518.2	E	57°	3110.9	790.1	E
10′	1926.4	315.2	.093	10′	2501.2	522.2	.151	10′	3121.7	795.2	.225
20′	1935.7	318.1		20′	2511.2	526.1		20′	3132.6	800.4	
30′	1945.0	321.1		30′	2521.1	530.1		30′	3143.4	805.6	
40′	1954.3	324.1		40′	2531.1	534.2		40′	3154.2	810.9	
50′	1963.6	327.1		50′	2541.0	538.2		50′	3165.1	816.1	
38°	1972.9	330.2		48°	2551.0	542.2		58°	3176.0	821.4	
10′	1982.2	333.2		10′	2561.0	546.3		10′	3186.9	826.7	
20′	1991.5	336.3	25° C.	20′	2571.0	550.4	25° C.	20′	3197.8	832.0	25° C.
30′	2000.9	339.3	T	30′	2581.0	554.5	T	30′	3208.8	837.3	T
40′	2010.2	342.4	.67	40′	2591.0	558.6	.85	40′	3219.7	842.7	1.05
50′	2019.6	345.5	E	50′	2601.1	562.8	E	50′	3230.7	848.1	E
39°	2029.0	348.6	.117	49°	2611.2	566.9	.189	59°	3241.7	853.5	.283
10′	2038.4	351.8		10′	2621.2	571.1		10′	3252.7	858.9	
20′	2047.8	354.9		20′	2631.3	575.3		20′	3263.7	864.3	
30′	2057.2	358.1		30′	2641.4	579.5		30′	3274.8	869.8	
40′	2066.6	361.3		40′	2651.5	583.8		40′	3285.8	875.3	
50′	2076.0	364.5		50′	2661.6	588.0		50′	3296.9	880.8	
40°	2085.4	367.7	30° C.	50°	2671.8	592.3	30° C.	60°	3308.0	886.4	30° C.
10′	2094.9	371.0	T	10′	2681.9	596.6	T	10′	3319.1	892.0	T
20′	2104.3	374.2	.80	20′	2692.1	600.9	1.02	20′	3330.3	897.5	1.27
30′	2113.8	377.5	E	30′	2702.3	605.3	E	30′	3341.4	903.2	E
40′	2123.3	380.8	.141	40′	2712.5	609.6	.227	40′	3352.6	908.8	
50′	2132.7	384.1		50′	2722.7	614.0		50′	3363.8	914.5	.340

T = R tan ½ I E = R exsec ½ I

Table IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=70°	I	T	E	I=80°	I	T	E	I=90°
61°	3375.0	920.2	+	71°	4086.9	1308.2	+	81°	4893.6	1805.3	+
10′	3386.3	925.9	5° C.	10′	4099.5	1315.6	5° C.	10′	4908.0	1814.7	5° C.
20′	3397.5	931.6	T	20′	4112.1	1322.9	T	20′	4922.5	1824.1	T
30′	3408.8	937.3	.25	30′	4124.8	1330.3	.30	30′	4937.0	1833.6	.36
40′	3420.1	943.1	E	40′	4137.4	1337.7	E	40′	4951.5	1843.1	E
50′	3431.4	948.9		50′	4150.1	1345.1		50′	4966.1	1852.6	
62°	3442.7	954.8	.080	72°	4162.8	1352.6	.110	82°	4980.7	1862.2	.149
10′	3454.1	960.6		10′	4175.6	1360.1		10′	4995.4	1871.8	
20′	3465.4	966.5		20′	4188.5	1367.6		20′	5010.0	1881.5	
30′	3476.8	972.4		30′	4201.2	1375.2		30′	5024.8	1891.2	
40′	3488.3	978.3		40′	4214.0	1382.8		40′	5039.5	1900.9	
50′	3499.7	984.3		50′	4226.8	1390.4		50′	5054.3	1910.7	
63°	3511.1	990.2	10° C.	73°	4239.7	1398.0	10° C.	83°	5069.2	1920.5	10° C.
10′	3522.6	996.2	T	10′	4252.6	1405.7	T	10′	5084.0	1930.4	T
20′	3534.1	1002.3	.51	20′	4265.6	1413.5	.61	20′	5099.0	1940.3	.72
30′	3545.6	1008.3	E	30′	4278.5	1421.2	E	30′	5113.9	1950.3	E
40′	3557.2	1014.4		40′	4291.5	1429.0		40′	5128.9	1960.2	
50′	3568.7	1020.5	.159	50′	4304.6	1436.8	.220	50′	5143.9	1970.3	.299
64°	3580.3	1026.6		74°	4317.6	1444.6		84°	5159.0	1980.4	
10′	3591.9	1032.8		10′	4330.7	1452.5		10′	5174.1	1990.5	
20′	3603.5	1039.0		20′	4343.8	1460.4		20′	5189.3	2000.6	
30′	3615.1	1045.2		30′	4356.9	1468.4		30′	5204.4	2010.8	
40′	3626.8	1051.4		40′	4370.1	1476.4		40′	5219.7	2021.1	
50′	3638.5	1057.7	15° C.	50′	4383.3	1484.4	15° C.	50′	5234.9	2031.4	15° C.
65°	3650.2	1063.9	T	75°	4396.5	1492.4	T	85°	5250.3	2041.7	T
10′	3661.9	1070.2	.76	10′	4409.8	1500.5	.91	10′	5265.6	2052.1	1.09
20′	3673.7	1076.6	E	20′	4423.1	1508.6	E	20′	5281.0	2062.5	E
30′	3685.4	1082.9	.240	30′	4436.4	1516.7	.332	30′	5296.4	2073.0	.450
40′	3697.2	1089.3		40′	4449.7	1524.9		40′	5311.9	2083.5	
50′	3709.0	1095.7		50′	4463.1	1533.1		50′	5327.4	2094.1	
66°	3720.9	1102.2		76°	4476.5	1541.4		86°	5343.0	2104.7	
10′	3732.7	1108.6		10′	4489.9	1549.7		10′	5358.6	2115.3	
20′	3744.6	1115.1		20′	4503.4	1558.0		20′	5374.2	2126.0	
30′	3756.5	1121.7		30′	4516.9	1566.3		30′	5389.9	2136.7	
40′	3768.5	1128.2	20° C.	40′	4530.4	1574.7	20° C.	40′	5405.6	2147.5	20° C.
50′	3780.4	1134.8	T	50′	4544.0	1583.1	T	50′	5421.4	2158.4	T
67°	3792.4	1141.4	1.02	77°	4557.6	1591.6	1.22	87°	5437.2	2169.2	1.45
10′	3804.4	1148.0	E	10′	4571.2	1600.1	E	10′	5453.1	2180.2	E
20′	3816.4	1154.7	.321	20′	4584.8	1608.6	.445	20′	5469.0	2191.1	.603
30′	3828.4	1161.3		30′	4598.5	1617.1		30′	5484.9	2202.2	
40′	3840.5	1168.1		40′	4612.2	1625.7		40′	5500.9	2213.2	
50′	3852.6	1174.8		50′	4626.0	1634.4		50′	5517.0	2224.3	
68°	3864.7	1181.6		78°	4639.8	1643.0		88°	5533.1	2235.5	
10′	3876.8	1188.4		10	4653.6	1651.7		10′	5549.2	2246.7	
20′	3889.0	1195.2	25° C.	20′	4667.4	1660.5	25° C.	20′	5565.4	2258.0	25° C.
30	3901.2	1202.0	T	30′	4681.3	1669.2	T	30′	5581.6	2269.3	T
40′	3913.4	1208.9	1.28	40′	4695.2	1678.1	1.53	40′	5597.8	2280.6	1.83
50′	3925.6	1215.8	E	50′	4709.2	1686.9	E	50′	5614.2	2292.0	E
69°	3937.9	1222.7	.403	79°	4723.2	1695.8	.558	89°	5630.5	2303.5	.756
10′	3950.2	1229.7		10′	4737.2	1704.7		10′	5646.9	2315.0	
20′	3962.5	1236.7		20′	4751.2	1713.7		20′	5663.4	2326.6	
30′	3974.8	1243.7		30′	4765.3	1722.7		30′	5679.9	2338.2	
40′	3987.2	1250.8		40′	4779.4	1731.7		40′	5696.4	2349.8	
50′	3999.5	1257.9		50′	4793.6	1740.8		50′	5713.0	2361.5	
70°	4011.9	1265.0	30° C.	80°	4807.7	1749.9	30° C.	90°	5729.7	2373.3	30° C.
10′	4024.4	1272.1	T	10′	4822.0	1759.0	T	10′	5746.3	2385.1	T
20′	4036.8	1279.3	1.54	20′	4836.2	1768.2	1.84	20′	5763.1	2397.0	2.20
30′	4049.3	1286.5	E	30′	4850.5	1777.4	E	30′	5779.9	2408.9	E
40′	4061.8	1293.6	.485	40′	4864.8	1786.7	.671	40′	5796.7	2420.9	.910
50′	4074.4	1300.9		50′	4879.2	1796.0		50′	5813.6	2432.9	

T = R tan ½ I E = R exsec ½ I

Table IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=100°	I	T	E	I=110°	I	T	E	I=120°
91°	5830.5	2444.9	+	101°	6950.6	3278.1	+	111°	8336.7	4386.1	+
10′	5847.5	2457.1	5° C.	10′	6971.3	3294.1	5° C.	10′	8362.7	4407.6	5° C.
20′	5864.6	2469.3	T	20′	6992.0	3310.1	T	20′	8388.9	4429.2	T
30′	5881.7	2481.5	.43	30′	7012.7	3326.1	.51	30′	8415.1	4450.9	.62
40′	5898.8	2493.8	E	40′	7033.6	3342.3	E	40′	8441.5	4472.7	E
50′	5916.0	2506.1		50′	7054.5	3358.5		50′	8468.0	4494.6	
92°	5933.2	2518.5	.200	102°	7075.5	3374.9	.268	112°	8494.6	4516.6	.360
10′	5950.5	2531.0		10′	7096.6	3391.2		10′	8521.3	4538.8	
20′	5967.9	2543.5		20′	7117.8	3407.7		20′	8548.1	4561.1	
30′	5985.3	2556.0		30′	7139.0	3424.3		30′	8575.0	4583.4	
40′	6002.7	2568.6		40′	7160.3	3440.9		40′	8602.1	4606.0	
50′	6020.2	2581.3		50′	7181.7	3457.6		50′	8629.3	4628.6	
93°	6037.8	2594.0	10° C.	103°	7203.2	3474.4	10° C.	113°	8656.6	4651.3	10° C.
10′	6055.4	2606.8	T	10′	7224.7	3491.3	T	10′	8684.0	4674.2	T
20′	6073.1	2619.7	.86	20′	7246.3	3508.2	.103	20′	8711.5	4697.2	1.25
30′	6090.8	2632.6	E	30′	7268.0	3525.2	E	30′	8739.2	4720.3	E
40′	6108.6	2645.5		40′	7289.8	3542.4		40′	8767.0	4743.6	
50′	6126.4	2658.5	.401	50′	7311.7	3559.6	.536	50′	8794.9	4766.9	.721
94°	6144.3	2671.6		104°	7333.6	3576.8		114°	8822.9	4790.4	
10′	6162.2	2684.7		10′	7355.6	3594.2		10′	8851.0	4814.1	
20′	6180.2	2697.9		20′	7377.8	3611.7		20′	8879.3	4837.8	
30′	6198.3	2711.2		30′	7399.9	3629.2		30′	8907.7	4861.7	
40′	6216.4	2724.5		40′	7422.2	3646.8		40′	8936.3	4885.7	
50′	6234.6	2737.9	15° C.	50′	7444.6	3664.5	15° C.	50′	8965.0	4909.9	15° C.
95°	6252.8	2751.3	T	105°	7467.0	3682.3	T	115°	8993.8	4934.1	T
10′	6271.1	2764.8	1.30	10′	7489.6	3700.2	1.56	10′	9022.7	4958.6	1.93
20′	6289.4	2778.3	E	20′	7512.2	3718.2	E	20′	9051.7	4983.1	E
30′	6307.9	2792.0	.604	30′	7534.9	3736.2	.806	30′	9080.9	5007.8	1.09
40′	6326.3	2805.6		40′	7557.7	3754.4		40′	9110.3	5032.6	
50′	6344.8	2819.4		50′	7580.5	3772.6		50′	9139.8	5057.6	
96°	6363.4	2833.2		106°	7603.5	3791.0		116°	9169.4	5082.7	
10′	6382.1	2847.0		10′	7626.6	3809.4		10′	9199.1	5107.9	
20′	6400.8	2861.0		20′	7649.7	3827.9		20′	9229.0	5133.3	
30′	6419.5	2875.0	20° C.	30′	7672.9	3846.5	20° C.	30′	9259.0	5158.8	20° C.
40′	6438.4	2889.0	T	40′	7696.3	3865.2	T	40′	9289.2	5184.5	T
50′	6457.3	2903.1	1.74	50′	7719.7	3884.0	2.08	50′	9319.5	5210.3	2.52
97°	6476.2	2917.3	E	107°	7743.2	3902.9	E	117°	9349.9	5236.2	E
10′	6495.2	2931.6	.809	10′	7766.8	3921.9	1.08	10′	9380.5	5262.3	1.46
20′	6514.3	2945.9		20′	7790.5	3940.9		20′	9411.3	5288.6	
30′	6533.4	2960.3		30′	7814.3	3960.1		30′	9442.2	5315.0	
40′	6552.6	2974.7		40′	7838.1	3979.4		40′	9473.2	5341.5	
50′	6571.9	2989.2		50′	7862.1	3998.7		50′	9504.4	5368.2	
98°	6591.2	3003.8		108°	7886.2	4018.2		118°	9535.7	5395.1	
10′	6610.6	3018.4	25° C.	10′	7910.4	4037.8	25° C.	10′	9567.2	5422.1	25° C.
20′	6630.1	3033.1	T	20′	7934.6	4057.4	T	20′	9598.9	5449.2	T
30′	6649.6	3047.9	2.18	30′	7959.0	4077.2	2.61	30′	9630.7	5476.5	3.16
40′	6669.2	3062.8	E	40′	7983.5	4097.1	E	40′	9662.6	5504.0	E
50′	6688.8	3077.7		50′	8008.0	4117.0		50′	9694.7	5531.7	
99°	6708.6	3092.7	1.02	109°	8032.7	4137.1	1.36	119°	9727.0	5559.4	1.83
10′	6728.4	3107.7		10′	8057.4	4157.3		10′	9759.4	5587.4	
20′	6748.2	3122.9		20′	8082.3	4177.5		20′	9792.0	5615.5	
30′	6768.1	3138.1		30′	8107.3	4197.9		30′	9824.8	5643.8	
40′	6788.1	3153.3		40′	8132.3	4218.4		40′	9857.7	5672.3	
50′	6808.2	3168.7		50′	8157.5	4239.0		50′	9890.8	5700.9	
100°	6828.3	3184.1	30° C.	110°	8182.8	4259.7	30° C.	120°	9924.0	5729.7	30° C.
10′	6848.5	3199.6	T	10′	8208.2	4280.5	T	10′	9957.5	5758.6	T
20′	6868.8	3215.1	2.62	20′	8233.7	4301.4	3.14	20′	9991.0	5787.7	3.81
30′	6889.2	3230.8	E	30′	8259.3	4322.4	E	30′	10025.0	5817.0	E
40′	6909.6	3246.5	1.22	40′	8285.0	4343.6	1.63	40′	10059.0	5846.5	2.20
50′	6930.1	3262.3		50′	8310.8	4364.8		50′	10093.0	5876.1	

T = R tan ½ I E = R exsec ½ I

Table X.

MIDDLE ORDINATES OF RAILS

Length of Rail (feet)

C ° ′	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch	C °	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch
0–20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0–40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1–0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1–20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1–40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2–0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2–20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2–40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3–0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3–20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3–40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4–0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4–20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4–40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

Table XI.

SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

Table XII.

INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise	Slope	Horizontal Distance	Correction	Rise
0°00′	100.000	0.000	0.000	8°00′	99.027	0.973	0.139
15′	99.999	0.001	0.004	15′	98.965	1.035	0.143
30′	99.996	0.004	0.009	30′	98.902	1.098	0.148
45′	99.991	0.009	0.013	45′	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

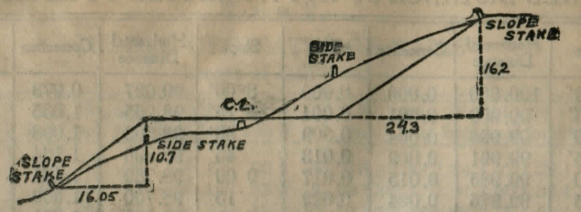
For each foot take one one-hundredth of each reading.

Table XIII.

MINUTES IN DECIMALS OF A DEGREE.

0 30″	.00833	10′ 30″	.17500	20′ 30″	.34167	30′ 10″	.50833	40′ 30″	.67500	50′ 10″	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000

#10 0+60.5 End of Top 8-1-51



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1½ TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	1.50	1 65	1 80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3 45	3.60	3 75	3.90	4.05	4.20	4 35	2
3	4.50	4 65	4.80	4.95	5.10	5 25	5 40	5.55	5.70	5.85	3
4	6.00	6 15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7 50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9 00	9 15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10 65	10.80	10.95	11.10	11.25	11.40	11.55	11 70	11.85	7
8	12.00	12 15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13 50	13.65	13 80	13 95	14.10	14.25	14.40	14 55	14.70	14.85	9
10	15.00	15 15	15 30	15 45	15.60	15.75	15.90	16.05	16.20	16 35	10
11	16 50	16 65	16 80	16.95	17 10	17.25	17.40	17.55	17.70	17.85	11
12	18 00	18.15	18.30	18 45	18.60	18 75	18.90	19.05	19.20	19.35	12
13	19 50	19 65	19.80	19.95	20.10	20.25	20 40	20.55	20.70	20.85	13
14	21.00	21 15	21.30	21.45	21 60	21.75	21.90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24 15	24 30	24 45	24.60	24.75	24 90	25 05	25.20	25.35	16
17	25.50	25 65	25.80	25 95	26.10	26 25	26 40	26.55	26.70	26.85	17
18	27.00	27 15	27.30	27 45	27.60	27.75	27.90	28.05	28 20	28.35	18
19	28 50	28 65	28 80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30 00	30 15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31 50	31 65	31.80	31.95	32 10	32 25	32.40	32.55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33.60	33 75	33.90	34.05	34.20	34.35	22
23	34 50	34 65	34.80	34.95	35.10	35 25	35 40	35.55	35.70	35 85	23
24	36.00	36 15	36.30	36 45	36.60	36.75	36.90	37.05	37 20	37.35	24
25	37.50	37.65	37 80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39 00	39 15	39.30	39 45	39 60	39.75	39.90	40.05	40.20	40.35	26
27	40 50	40 65	40 80	40.95	41.10	41.25	41 40	41.55	41.70	41.85	27
28	42 00	42 15	42.30	42.45	42.60	42 75	42.90	43.05	43.20	43.35	28
29	43 50	43 65	43.80	43 95	44.10	44 25	44 40	44.55	44.70	44 85	29
30	45 00	45 15	45.30	45 45	45.60	45.75	45.90	46.05	46 20	46.35	30
31	46.50	46.65	46.80	46 95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48 00	48.15	48.30	48 45	48.60	48 75	48.90	49.05	49 20	49.35	32
33	49.50	49 65	49.80	49.95	50.10	50.25	50.40	50.55	50 70	50.85	33
34	51 00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52 50	52.65	52.80	52.95	53.10	53.25	53.40	53.55	53.70	53.85	35
36	54 00	54.15	54.30	54 45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55 50	55 65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57 45	57.60	57 75	57.90	58.05	58.20	58 35	38
39	58 50	58.65	58 80	58 95	59.10	59 25	59.40	59 55	59.70	59.85	39
40	60 00	60 15	60 30	60 45	60 60	60.75	60 90	61.05	61 20	61.35	40
41	61.50	61 65	61 80	61 95	62 10	62 25	62.40	62 55	62 70	62.85	41
42	63 00	63.15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64.35	42
43	64.50	64 65	64 80	64.95	65.10	65 25	65 40	65.55	65.70	65.85	43
44	66 00	66 15	66 30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67 50	67 65	67 80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69 00	69 15	69 30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70 50	70 65	70 80	70 95	71.10	71.25	71 40	71.55	71.70	71.85	47
48	72.00	72 15	72.30	72.45	72.60	72.75	72.90	73 05	73.20	73 35	48
49	73 50	73 65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

Computed by L. Leland Locke.

0.91

11/14/50 936.50 13496.43 53.07

M. Kotelos
"Egg-Orchard Farm"
1000 ft W of d W. Matthews
5th side Music
Sewer & orchard Es
side house

TABLE OF INCHES REDUCED TO DECIMALS OF A FOOT.

Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.
1/16	.0052	5/16	.1094	9/16	.2135	13/16	.3177	1/16	.4219	5/16	.5260	9/16	.6302	13/16	.7344	1/16	.8385	5/16	.9427
1/8	.0104	3/8	.1146	5/8	.2188	7/8	.3229	1/8	.4271	3/8	.5313	5/8	.6354	7/8	.7396	1/8	.8438	3/8	.9479
3/16	.0156	7/16	.1198	11/16	.2240	15/16	.3281	3/16	.4323	7/16	.5365	11/16	.6406	15/16	.7448	3/16	.8490	7/16	.9531
1/4	.0208	1/2	.1250	3/4	.2292	4—	.3333	1/4	.4375	1/2	.5417	3/4	.6458	9—	.7500	1/4	.8542	1/2	.9583
5/16	.0260	9/16	.1302	13/16	.2344	1/16	.3385	5/16	.4427	9/16	.5469	13/16	.6510	1/16	.7552	5/16	.8594	9/16	.9635
3/8	.0313	5/8	.1354	7/8	.2396	1/8	.3438	3/8	.4479	5/8	.5521	7/8	.6563	1/8	.7604	3/8	.8646	5/8	.9688
7/16	.0365	11/16	.1406	15/16	.2448	3/16	.3490	7/16	.4531	11/16	.5573	15/16	.6615	3/16	.7656	7/16	.8698	11/16	.9740
1/2	.0417	3/4	.1458	3—	.2500	1/4	.3542	1/2	.4583	3/4	.5625	8—	.6667	1/4	.7708	1/2	.8750	3/4	.9792
9/16	.0469	13/16	.1510	1/16	.2552	5/16	.3594	9/16	.4635	13/16	.5677	1/16	.6719	5/16	.7760	9/16	.8802	13/16	.9844
5/8	.0521	7/8	.1563	1/8	.2604	3/8	.3646	5/8	.4688	7/8	.5729	1/8	.6771	3/8	.7813	5/8	.8854	7/8	.9896
11/16	.0573	15/16	.1615	3/16	.2656	7/16	.3698	11/16	.4740	15/16	.5781	3/16	.6823	7/16	.7865	11/16	.8906	15/16	.9948
3/4	.0625	4—	.1667	1/4	.2708	1/2	.3750	3/4	.4792	7—	.5833	1/4	.6875	1/2	.7917	3/4	.8958		
13/16	.0677	1/16	.1719	5/16	.2760	9/16	.3803	13/16	.4844	1/16	.5885	5/16	.6927	9/16	.7969	13/16	.9010		
7/8	.0729	1/8	.1771	3/8	.2813	5/8	.3854	7/8	.4896	1/8	.5938	3/8	.6979	5/8	.8021	7/8	.9063		
15/16	.0781	3/16	.1823	7/16	.2865	11/16	.3906	15/16	.4948	3/16	.5990	7/16	.7031	11/16	.8073	15/16	.9115		
1—	.0833	1/4	.1875	1/2	.2917	3/4	.3958	6—	.5000	1/4	.6042	1/2	.7083	10—	.8125	11—	.9167		
1/16	.0885	5/16	.1927	9/16	.2969	13/16	.4010	1/16	.5052	5/16	.6094	9/16	.7135	1/16	.8177	1/16	.9219		
1/8	.0938	3/8	.1979	5/8	.3021	7/8	.4063	1/8	.5104	3/8	.6146	5/8	.7188	1/8	.8229	1/8	.9271		
3/16	.0990	7/16	.2031	11/16	.3073	15/16	.4115	3/16	.5156	7/16	.6198	11/16	.7240	3/16	.8281	3/16	.9323		
1/4	.1042	1/2	.2083	3/4	.3125	5—	.4167	1/4	.5208	1/2	.6250	3/4	.7292	1/4	.8333	1/4	.9375		

B. K. ELLIOTT COMPANY, PITTSBURG, PA.
DRAWING MATERIALS AND SURVEYING INSTRUMENTS